



TRENDELENBURG, DUCHENNE **EN BALANS**







A



B



C

Ueber den

Gang bei angeborener Hüftgelenksluxation.

Von

Prof. F. Trendelenburg.

„Deutschen Medicinischen Wochenschrift“ 1895, No. 2.
Prof. Dr. A. Eulenborg und Dr. Jul. Schwalbe.

Leipzig.

Verlag von Georg Thieme.

1895



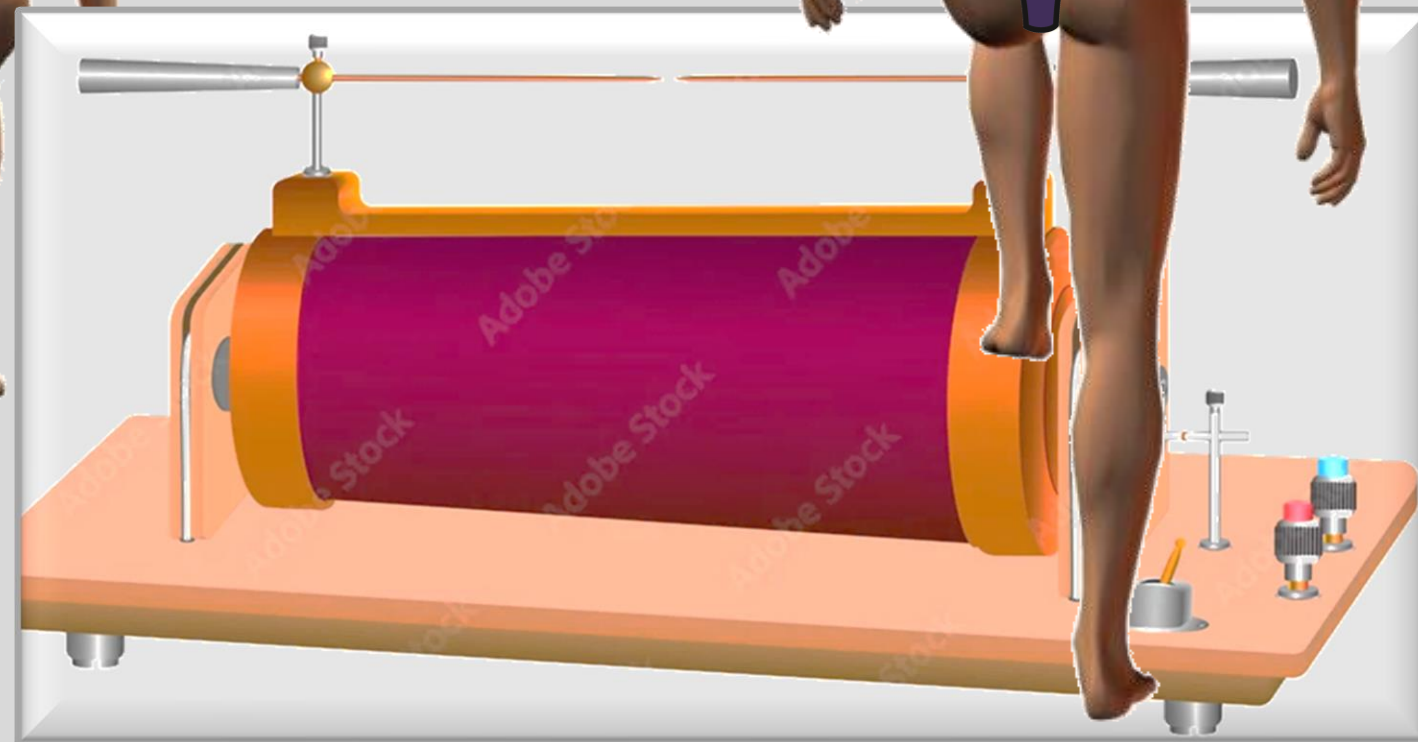
PHYSIOLOGIE DES MOUVEMENTS DÉMONTRÉE

A L'AIDE DE L'EXPÉRIMENTATION CLINIQUE

ET DE L'OBSERVATION CLINIQUE
ET APPLICABLE

À L'ÉTUDE DES PARALYSIES ET DES DÉVIATIONS

PAR LE DOCTEUR
G. B. DUCHENNE (DE BOULOGNE)



In welke fase van de gangcyclus treden deze storingen op?

Beide storingen treden op in de unipedale standfase van het aangedane been (dus tijdens de zwaai fase van het niet-aangedane been).

Aangedane been?
LINKS



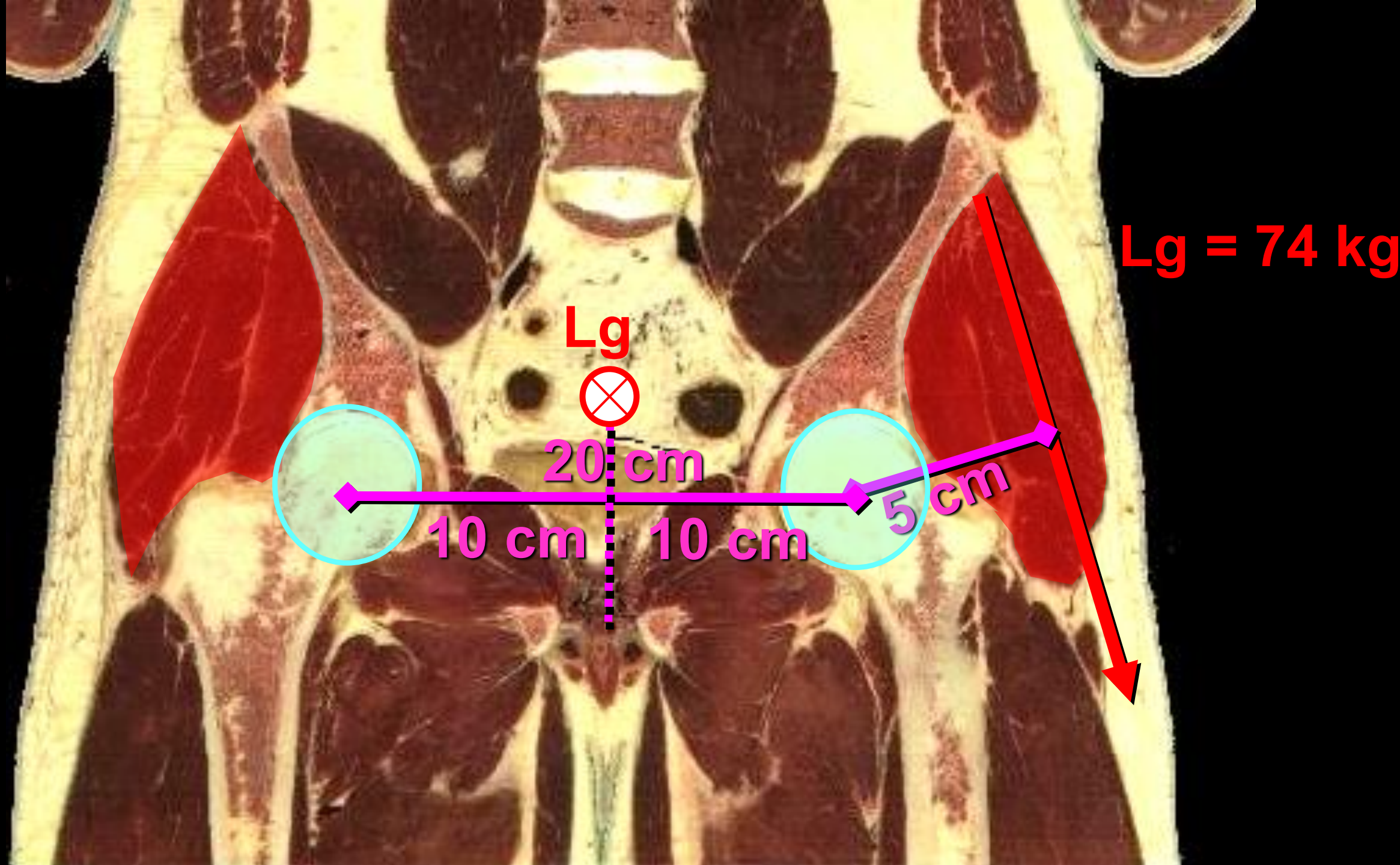
Aangedane been?
RECHTS



Welke oorzaken zijn er voor deze gangpatronen ?



Wat zijn de voorwaarden om op 1 been te kunnen staan?



Lg

20 cm

10 cm

10 cm

5 cm

$Lg = 74\text{ kg}$

Stand op 1 been:
Inwendig evenwicht

$L_g = 74 \text{ kg}$

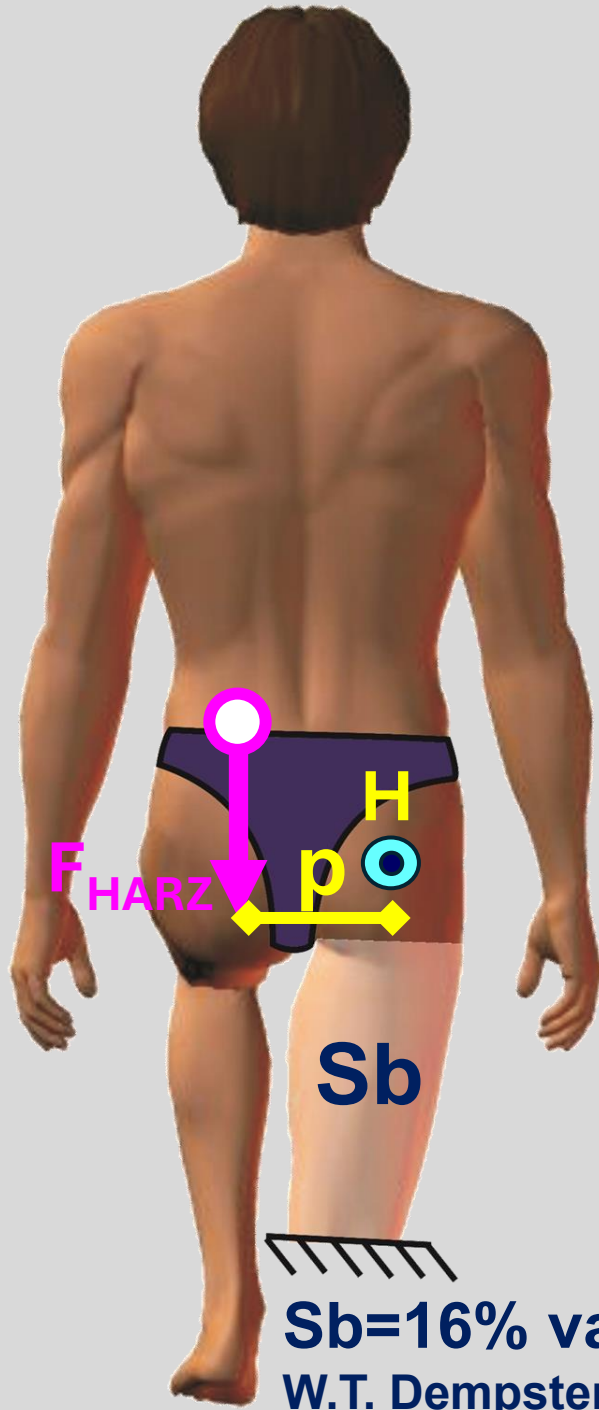
$F_{\text{HARZ}} = 74 - 12 = 62 \text{ kg}$

$P = 12 \text{ cm}$

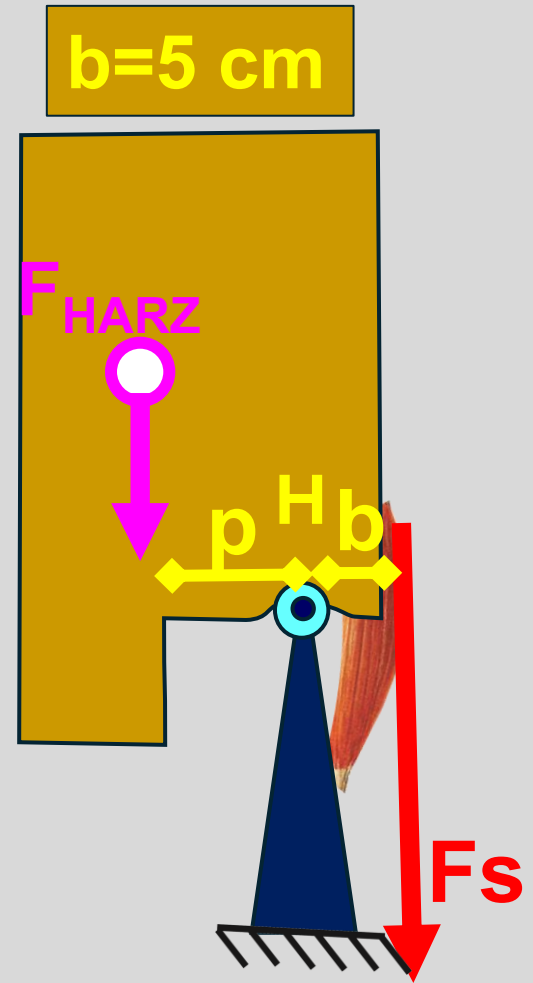
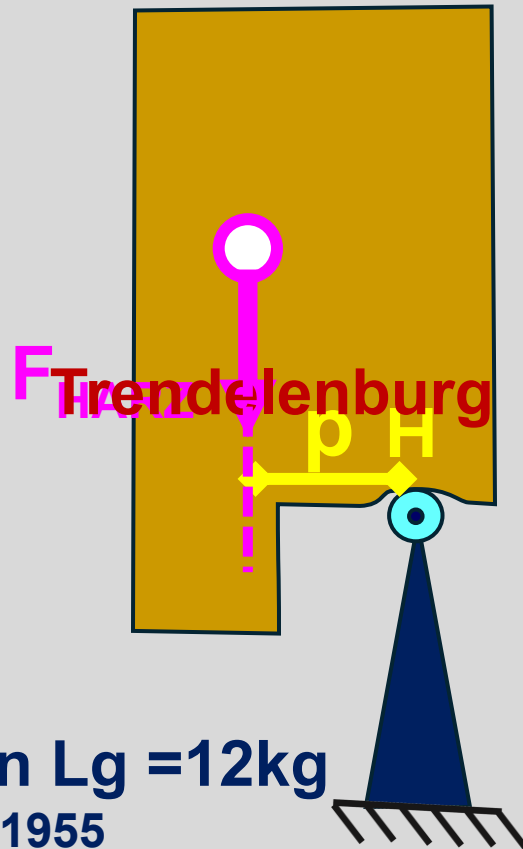
$$F_s \times b = F_{\text{HARZ}} \times p$$

$$F_s = (62 \times 12) / 5$$

$$= 148 \text{ kgf}$$



$S_b = 16\% \text{ van } L_g = 12 \text{ kg}$
W.T. Dempster 1955

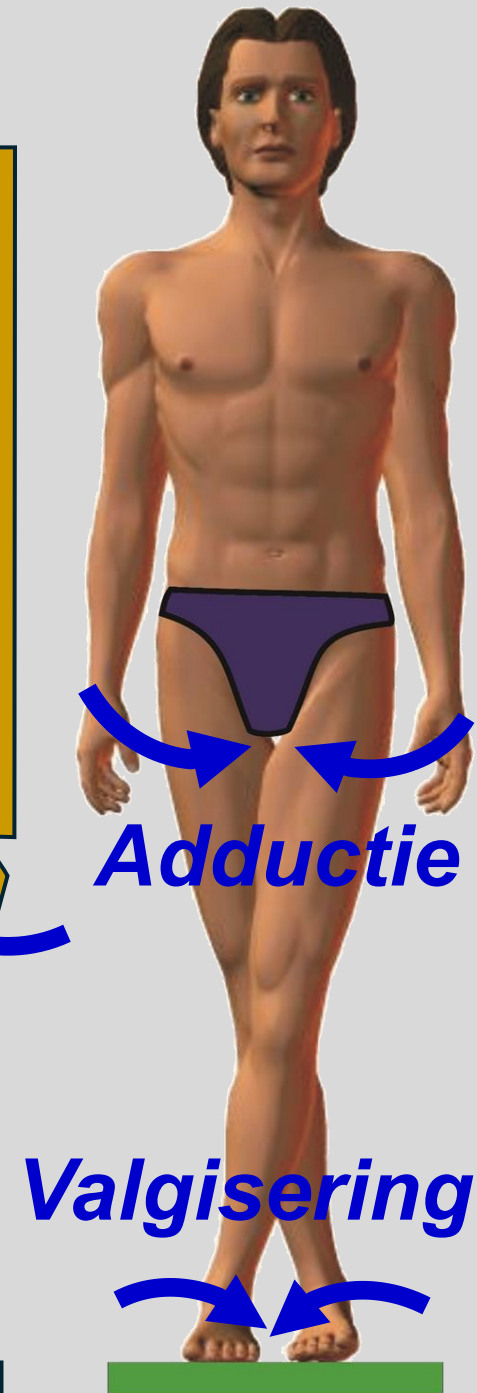
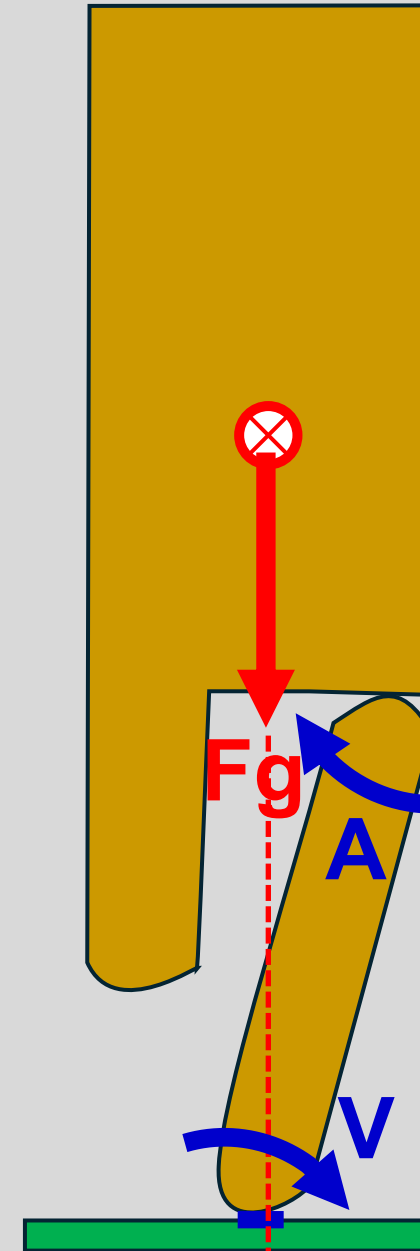
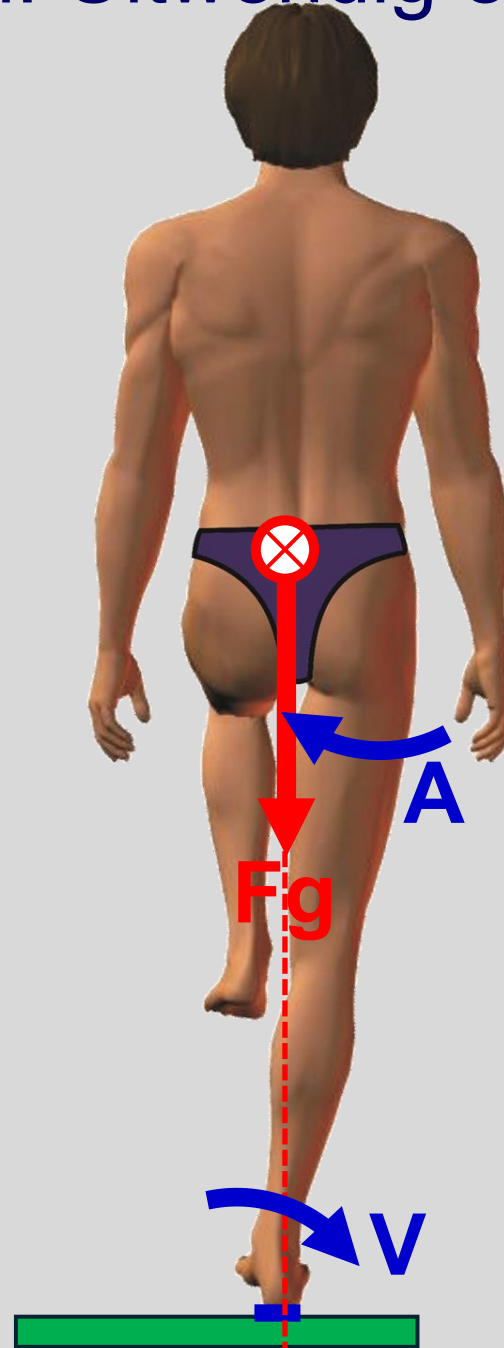
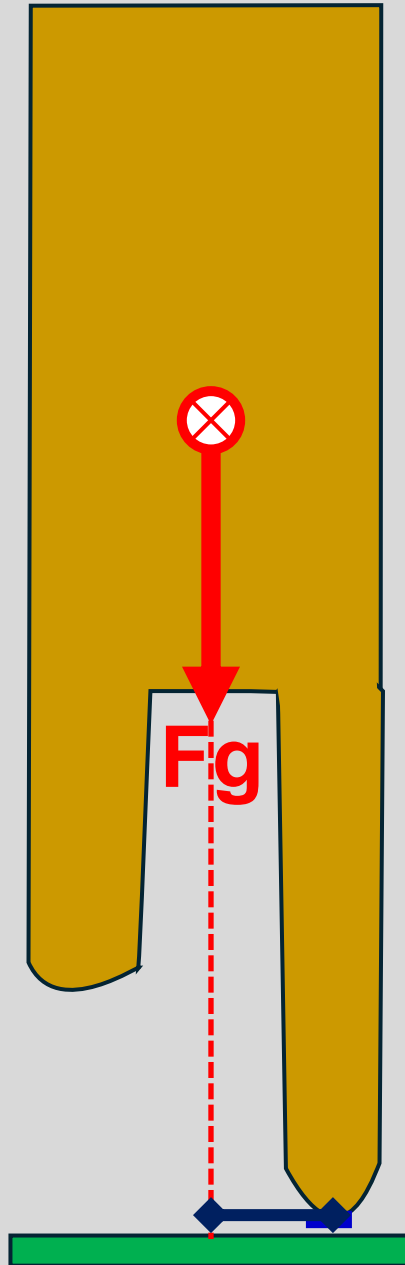
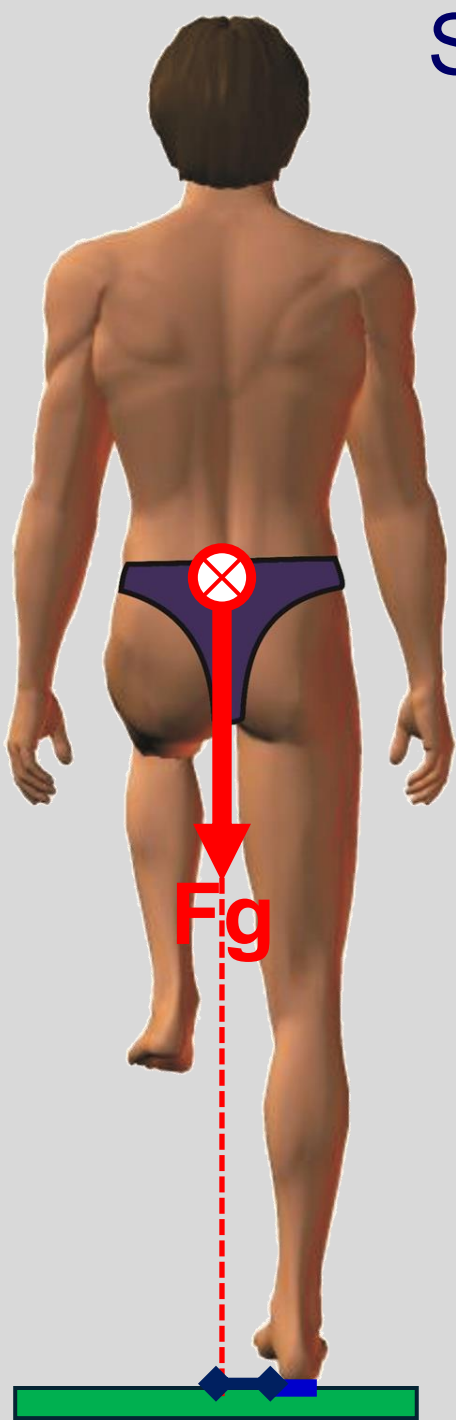


$b = 5 \text{ cm}$

UITWENDIG EVENWICHT: ZWAARTEPUNT EN STEUNVLAK

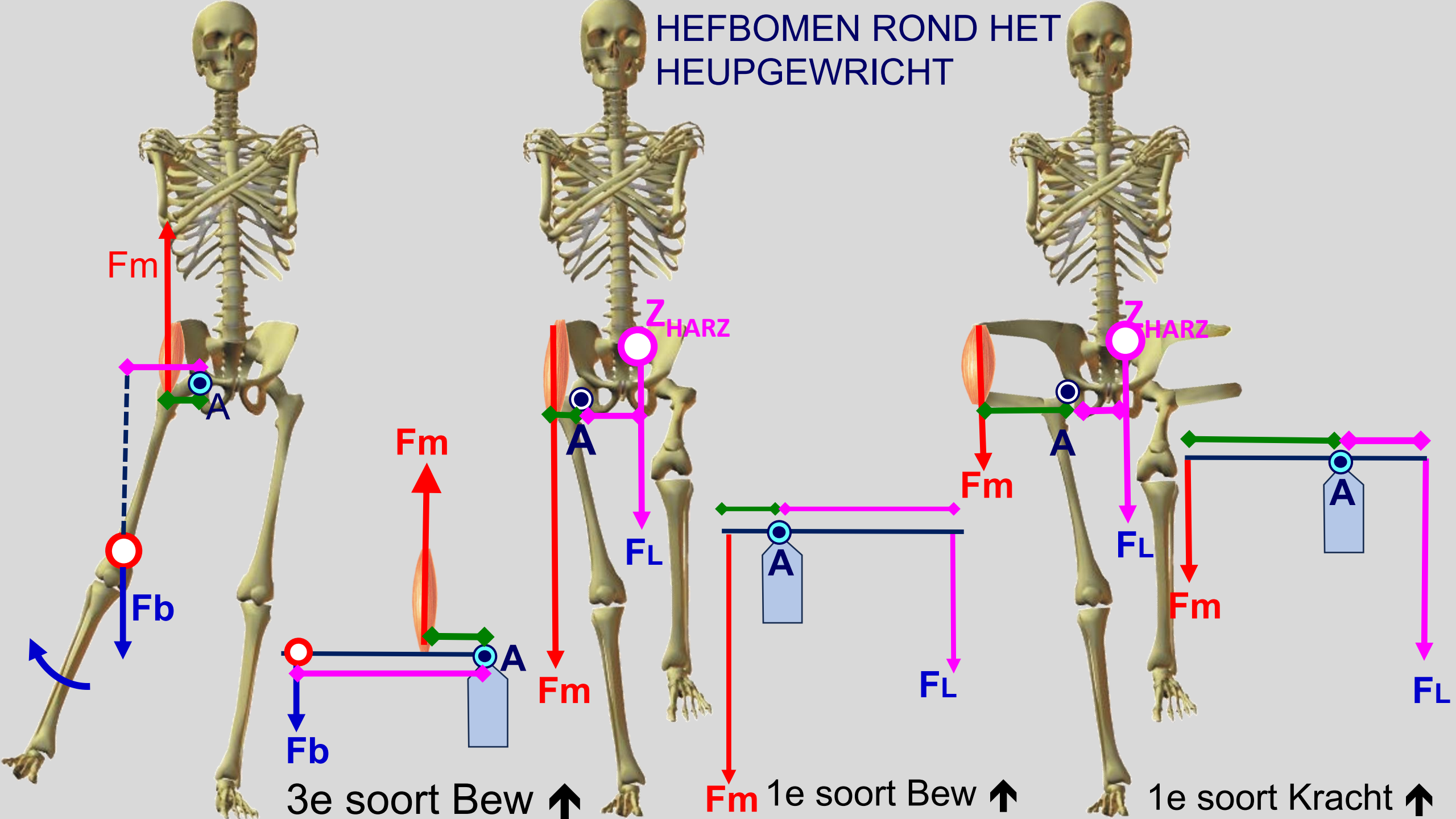


Stand op 1 been: Uitwendig evenwicht



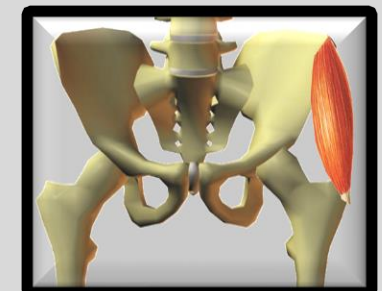
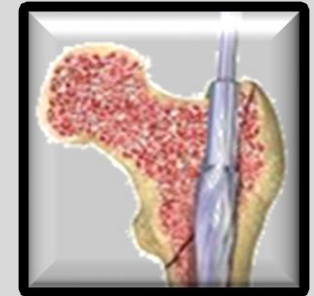
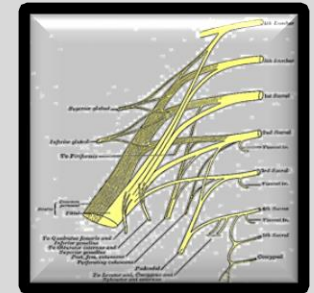
HEFBOMEN
rond het heupgewricht

HEFBOMEN ROND HET HEUPGEWRIGHT



Oorzaken van onvoldoende abducerende momenten rond het heupgewricht van het standbeen:

- *parese/paralyse van de heupabductoren;*
- *beschadiging heupabductoren → contractie pijnlijk;*
- *een intraossale veneuze hypertensie in de femurkop bij coxarthrosis deformans;*
- *een vermindering van de origo-insertie-afstand en/of een verkleining van de momentsarm van de heupabductoren.*



Criteria voor de beoordeling van de Trendelenburg-test (abductoren rechts).

Criterium 1:

Het bekken *moet stijgen*:
zo ja positief, zo nee
negatief.

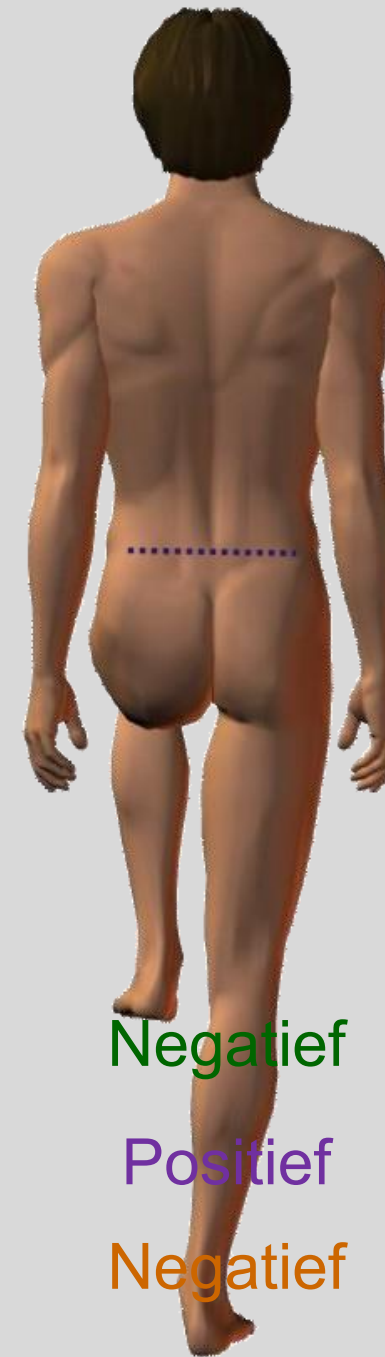
Criterium 2:

Het bekken *moet horizontaal
blijven*: zo ja positief, zo nee
negatief.

Criterium 3:

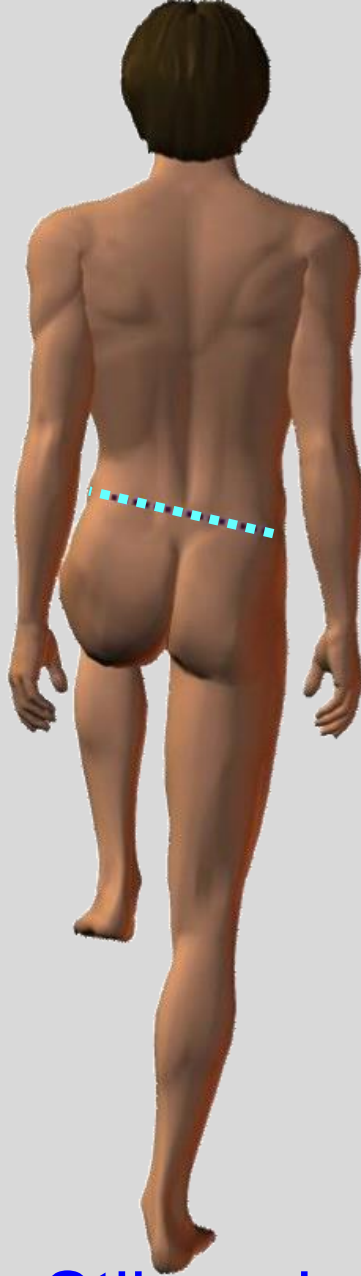
Het bekken *mag niet dalen*: zo ja
positief, zo nee negatief.

**Een positieve of negatieve Trendelenburg
kan dus alles betekenen: bekken stijgt,
bekken horizontaal, bekken daalt.**

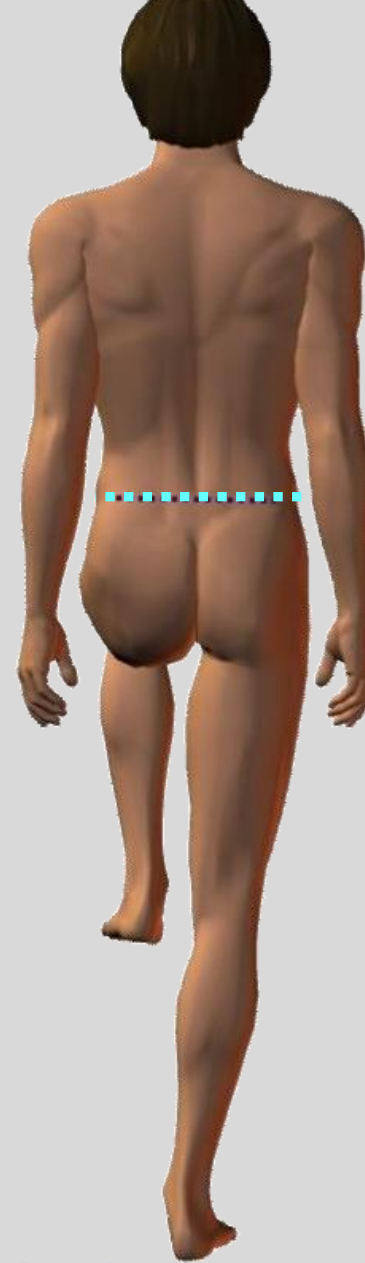


Criteria voor de beoordeling
van de Trendelenburg-test.

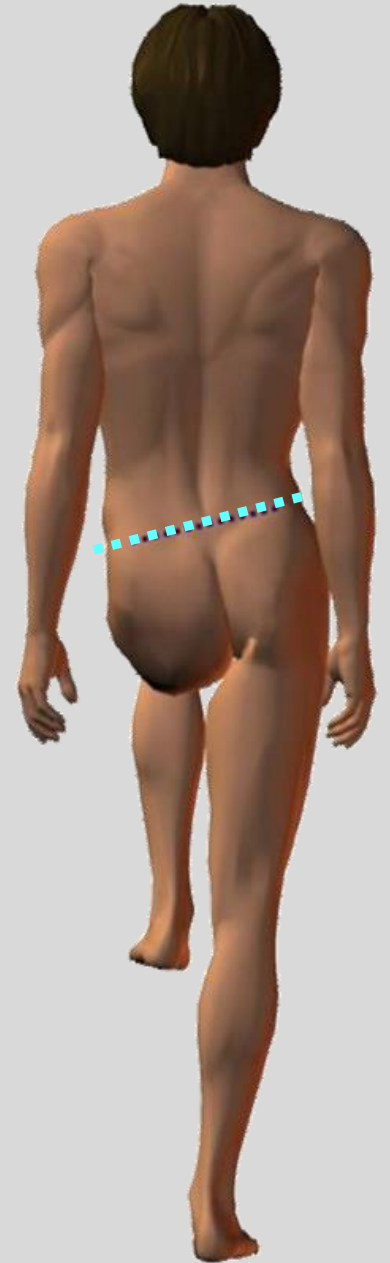
Voorstel:
De beschrijvende
Trendelenburg-score.



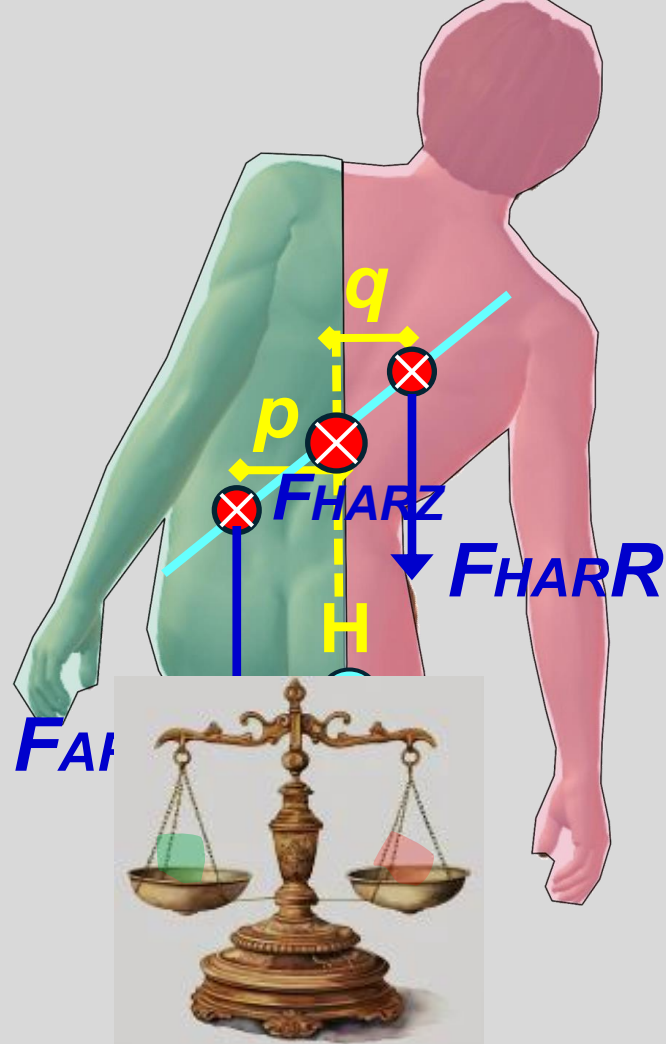
Stijgende
Trendelenburg



Horizontale
Trendelenburg



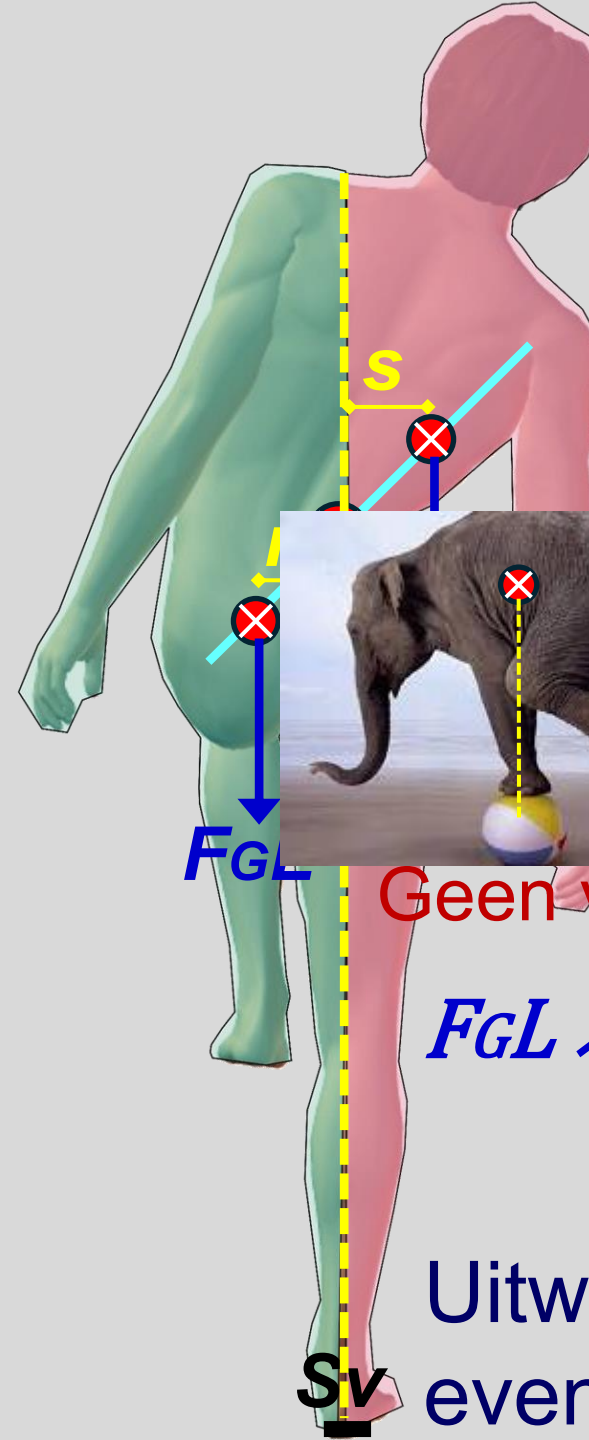
Dalende
Trendelenburg



$$F_{ARZL} \times p = F_{HARR} \times q$$

Geen abductoren nodig!

Inwendig
evenwicht



Hoe werkt de gang
van Duchenne?



uctie heup nodig!
Geen valgus enkel nodig!

$$F_{GL} \times r = F_{GR} \times s$$

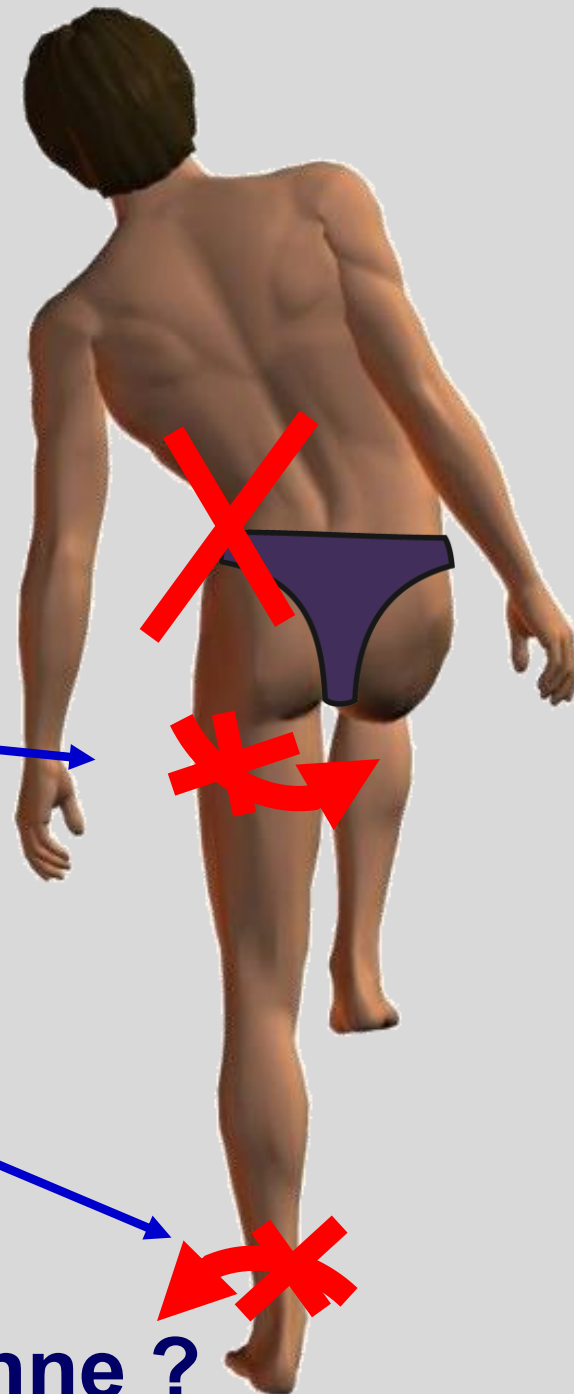
Uitwendig
evenwicht



Onvoldoende F
abductoren

Onvoldoende
adductie heup

Onvoldoende
valgisering enkel

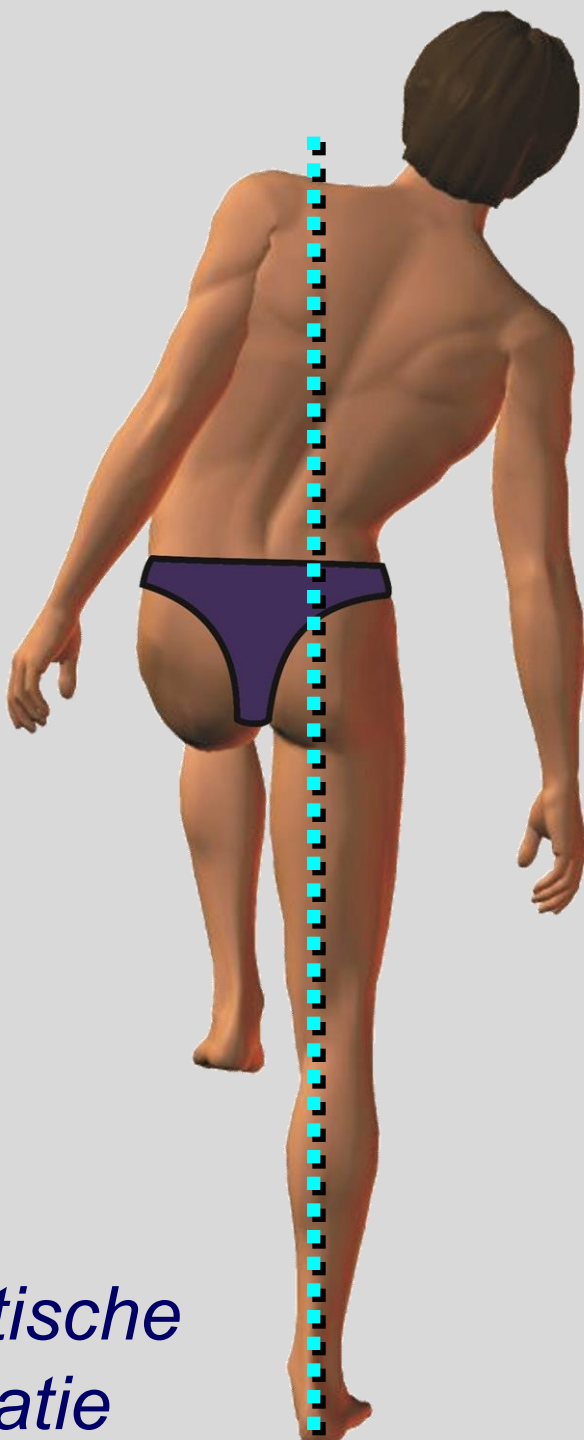


Trendelenburg ?

of

Duchenne ?

*Statische
situatie*



Dynamische situatie:
de rompuitwijking is
veel minder groot dan
in de statische
situatie!

Zelfs bij zeer lage
gangsnelheden (ca. 1
km/uur) wordt een
gang van Duchenne
al gemaskeerd!

Relatief geringe steun
kan de Duchenne
volledig maskeren.

*Dynamische
situatie*



Ontlasting van enkel / knie en heup door een wandelstok

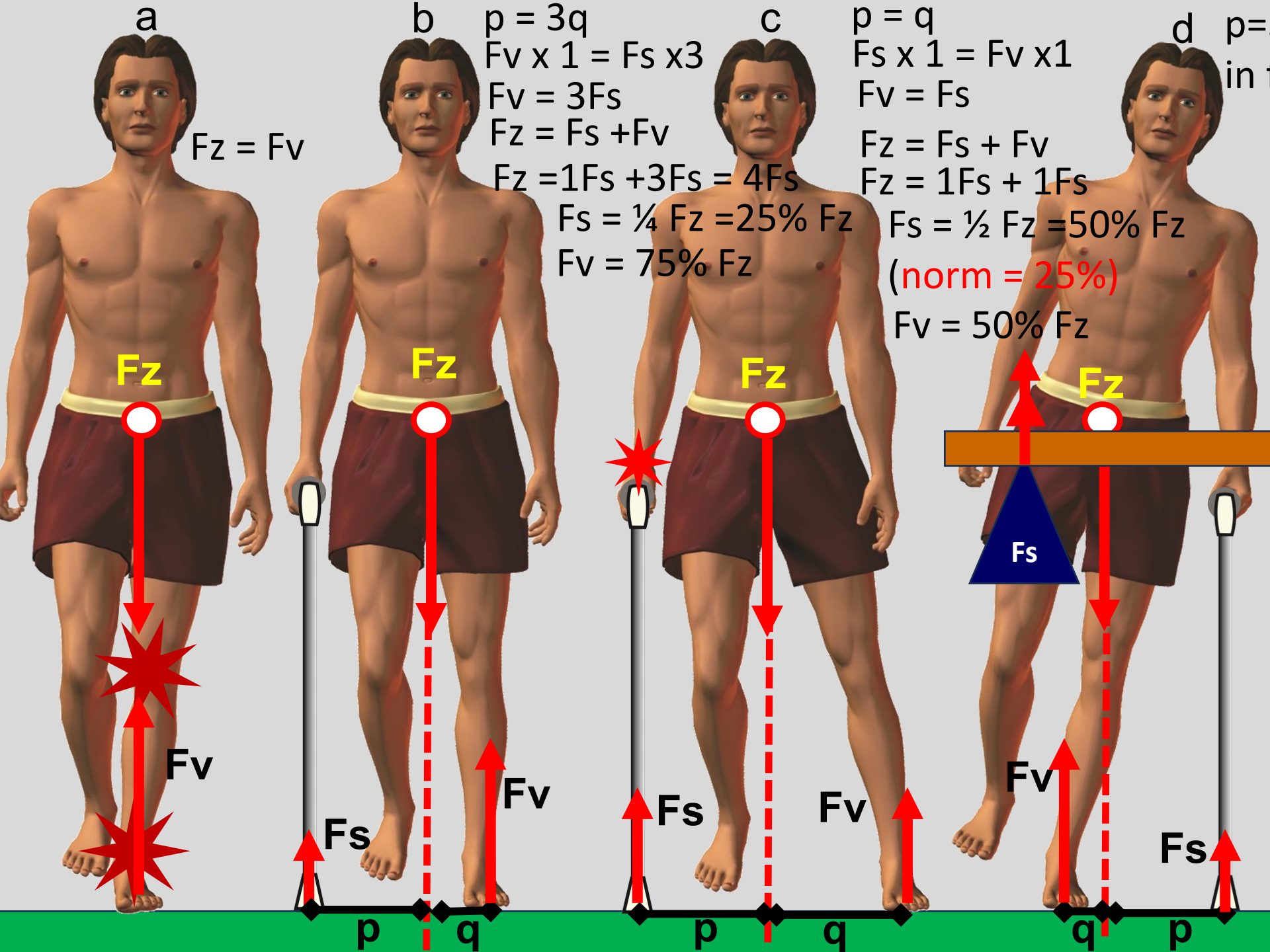




Steunvlak en maximale belasting op een handvat

Maximale belasting handvat ($L_g = 74 \text{ kg}$):
 $11 - 34 \% L_g = 8 - 25 \text{ kgf}$
Gemiddeld: **25% $L_g = 18,5 \text{ kgf}$**

14. Anglin C, Wyss U. Arm motion and load analysis of sit-to-stand, stand-to-sit, cane walking and lifting. ClinBiomech. 2000;15(6):441–8.
15. Aragaki D, Nasmyth M, Schultz S, Nguyen G, Yentes J, Kao K, Perell K, Fang M. Immediate effects of contralateral and ipsilateral cane use on normal adult gait. PM R. 2009;1(3):208–13.
16. Brand R, Crowninshield R. The effect of cane use on hip contact force. ClinOrthopRelatRes. 1980;147:181–3.
17. Deckers J, Beckers D. Ganganalyse en looptraining voor de paramedicus. Houten/Diegem: Bohn Stafleu van Loghum; 1996.
18. Fang M, Heiney C, Yentes J, Harada N, Masih S, Perell-Gerson K. Effects of contralateral versus ipsilateral cane use on gait in people with knee osteoarthritis. PM R. 2015;7:400–6.
19. Lyu S, Ogata K, Hoshiko I. Effects of a cane on floor reaction force and center of force during gait. Clin OrthopRelatRes. 2000;375:313–9.
20. Sherif S, Hasan S, Arnold G, Abboud R, Wang W. Analysis of hand pressure in different crutch lengths and upperlimb movements during crutch walking. Int J Ind Ergon. 2016;53:59–66.
21. Winter D, Deathe A, Halliday S, Ishac M, Olin M. A technique to analyse the kinetics and energetics of cane-assisted gait. ClinBiomech. 1993;8:37–43.
22. Youdas J, Kotajarvi B, Padgett J, Kaufman K. Partial weight bearing gait using conventional assistive devices. ArchPhys MedRehabil. 2005;86:394–8.
23. Youdas J, Kotajarvi B, Padgett J, Kaufman K. Partial weight-bearing gait using conventional assistive devices. Arch Phys Med Rehabil 2005;86:394-8.



HEUP- ONTLASTING

$L_g = 74 \text{ kg}$

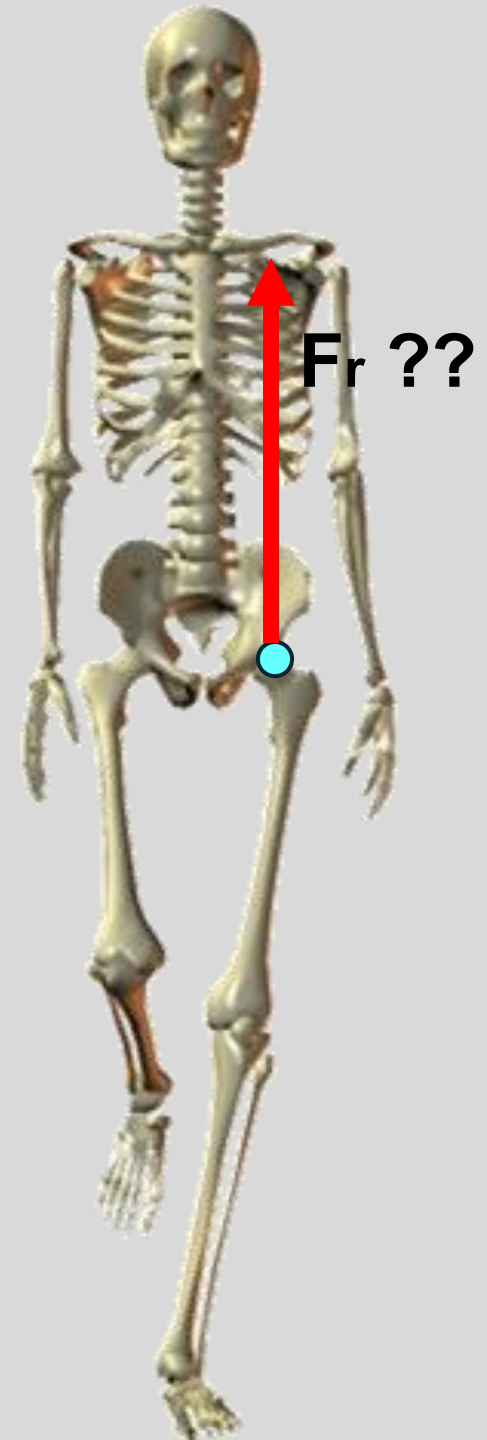
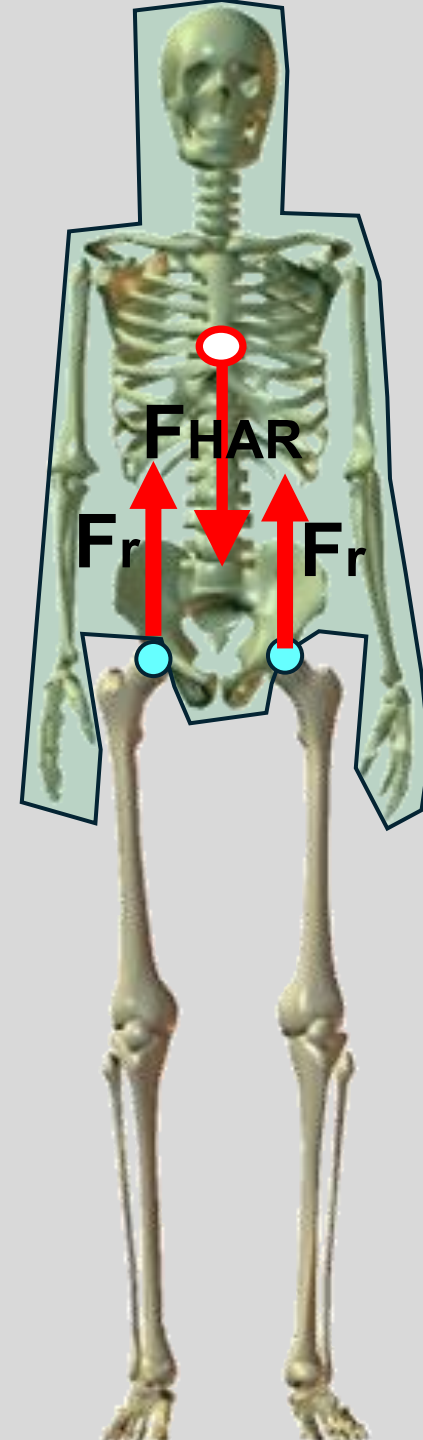
Been = 16% van $L_g = 12 \text{ kg}$

$$F_{HAR} = 74 - (2 \times 12) = 50 \text{ kgf}$$

Wat is de belasting van de heupgewrichten (F_r)?

$$50 \div 2 = 25 \text{ kgf}$$

Stand op één been:
wat is nu de belasting van het heupgewricht ?



HEUP-ONTLASTING

$$F_g = 74 \text{ kgf} \rightarrow F_{\text{harz}} 62 \text{ kgf}$$

$$p = 12 \text{ cm} \quad q = 5 \text{ cm}$$

$$F_s \times q = F_{\text{harz}} \times p$$

$$F_s = (F_{\text{harz}} \times p) / q$$

$$F_s = (62 \times 12) / 5 = 148 \text{ kgf}$$

$$F_r = F_{\text{harz}} + F_s = 62 + 148 = 210 \text{ kgf}$$

$$F_h = 25\% \text{ van } F_g = 18,5 \text{ kgf}$$

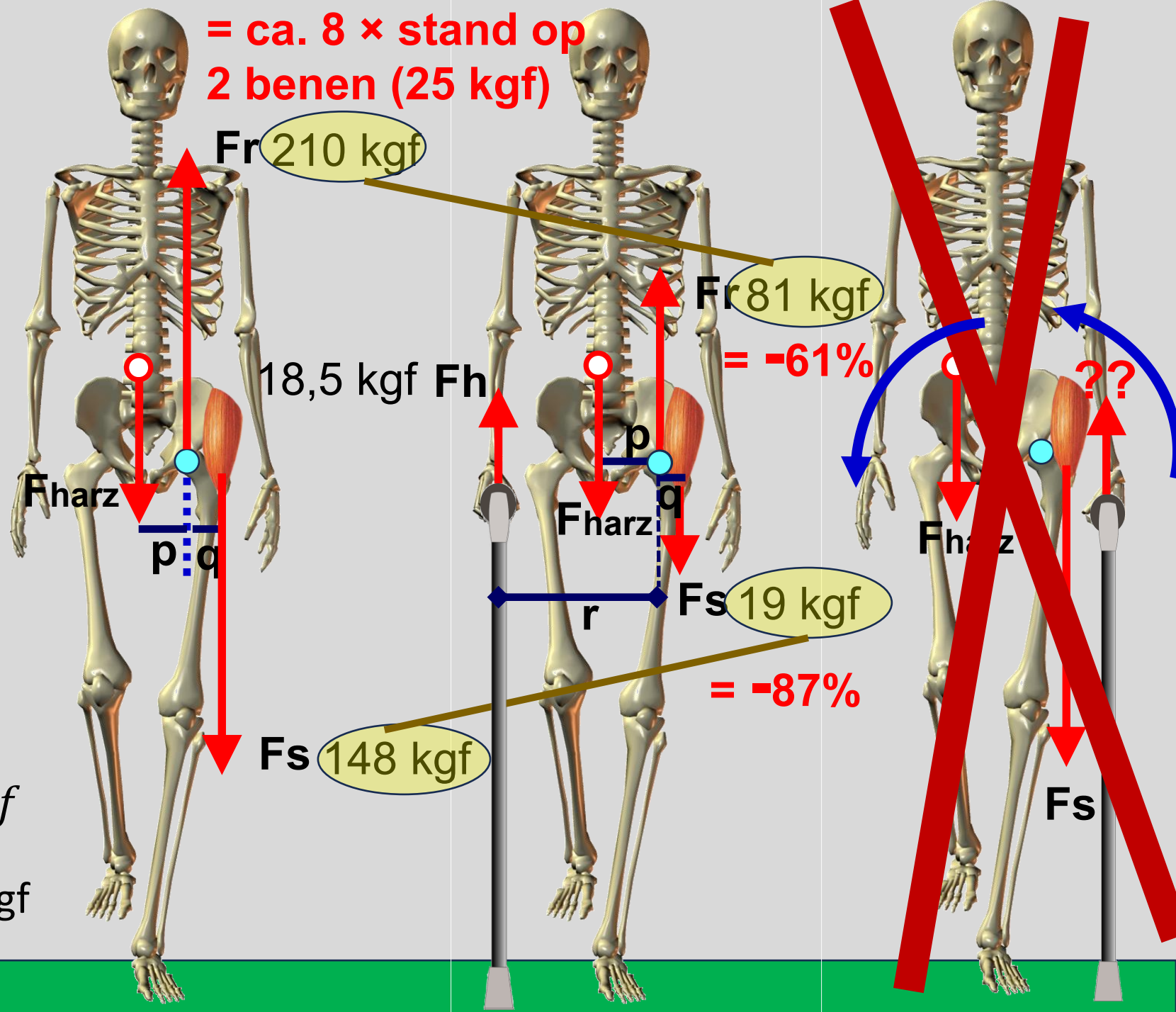
$$r = 35 \text{ cm} \quad q = 5 \text{ cm}$$

$$F_s \times q + F_h \times r = F_{\text{harz}} \times p$$

$$F_s = \frac{62 \times 12 - 18,5 \times 35}{5} = 19 \text{ kgf}$$

$$F_r = F_{\text{harz}} + F_s = 62 + 19 = 81 \text{ kgf}$$

= ca. 8 × stand op
2 benen (25 kgf)



HEUP- ONTLASTING DOOR TOEVOEGEN VAN EEN LAST

Ter vergelijik:

$$Flast = 14,5 \text{ kgf} \quad r = 25 \text{ cm}$$

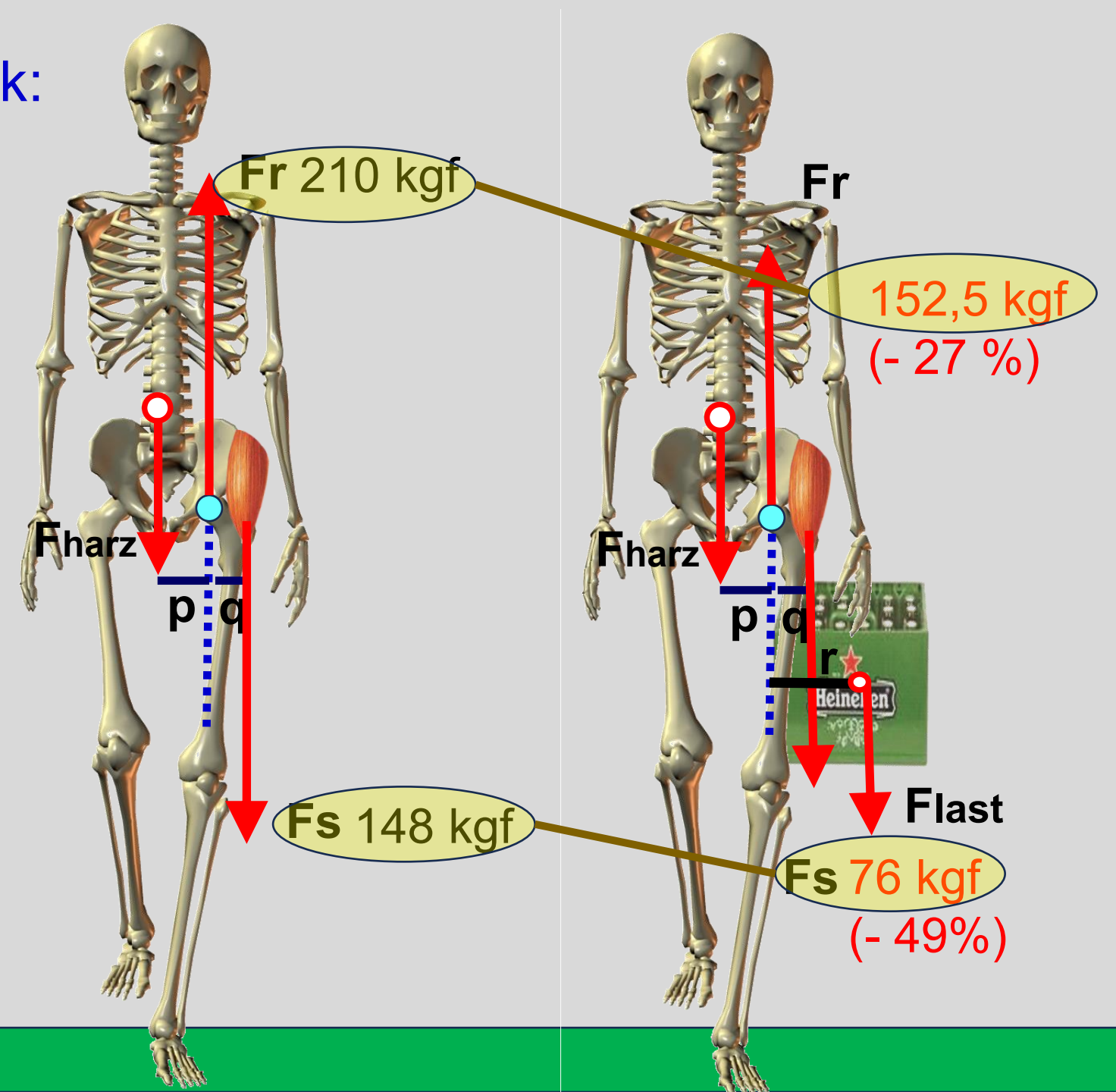
$$Fs \times q + Flast \times r = Fharz \times p$$

$$Fs = (Fharz \times p - Flast \times r) / q$$

$$Fs = (62 \times 12 - 14,5 \times 25) / 5 = 76 \text{ kgf}$$

$$Fr = Fs + Fharz + Flast$$

$$Fr = 76 + 62 + 14,5 = 152,5 \text{ kgf}$$



De wandelstok en balans



Handvatvormen

Rondhaak
(schaap-
herder)



Recht
hoekig

Derby
of
Fritz

Derby



Ergonomic Grip

Enhanced
Stability

Classic Design

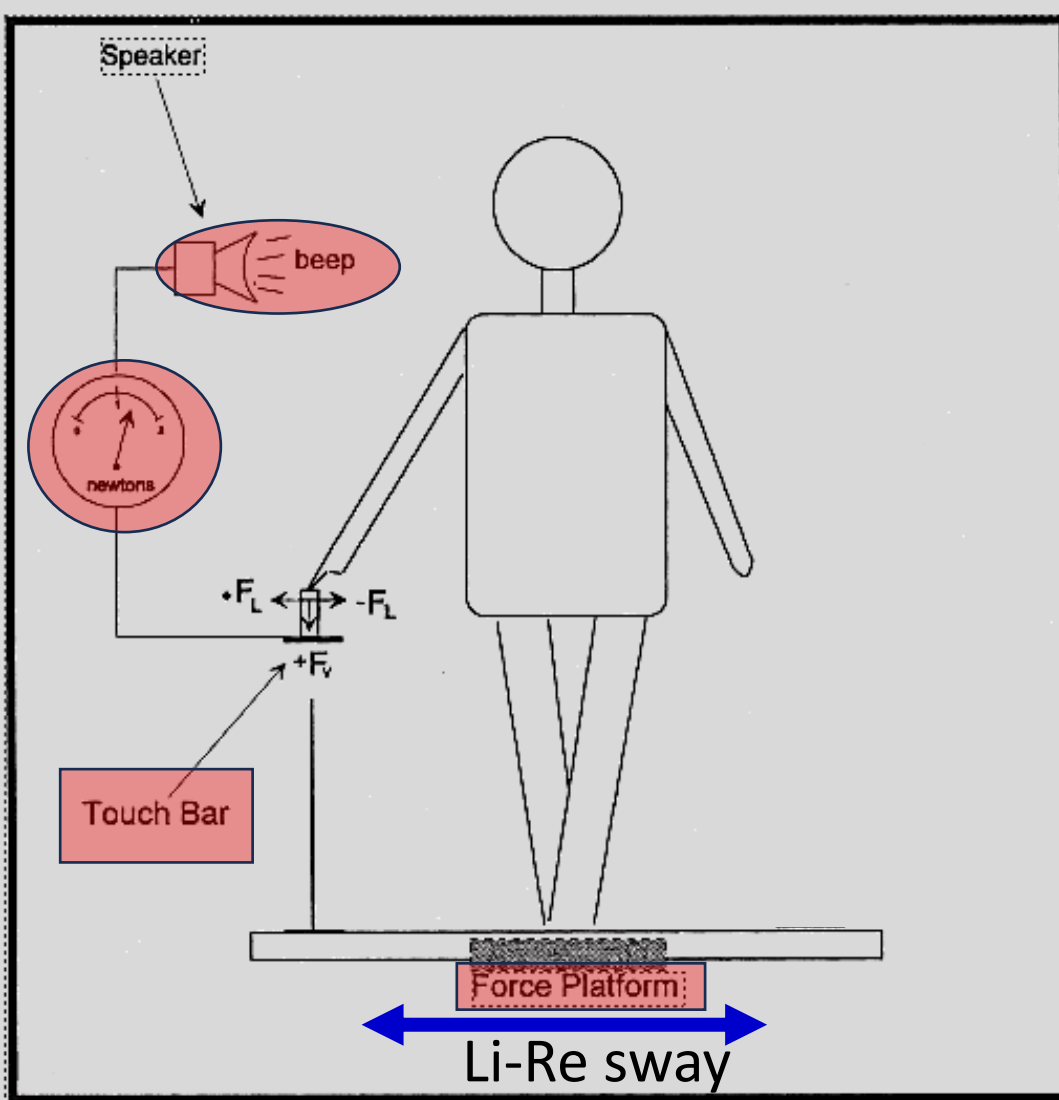
Fritz



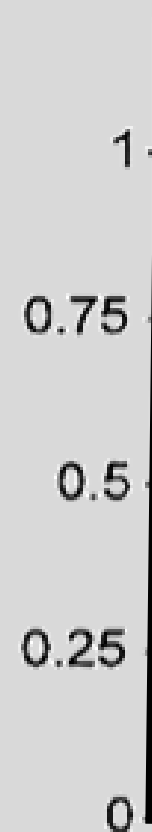
Even Pressure
Distribution

Arthritis Relief

Sleek Design



Mean COPx Displacement (cm)

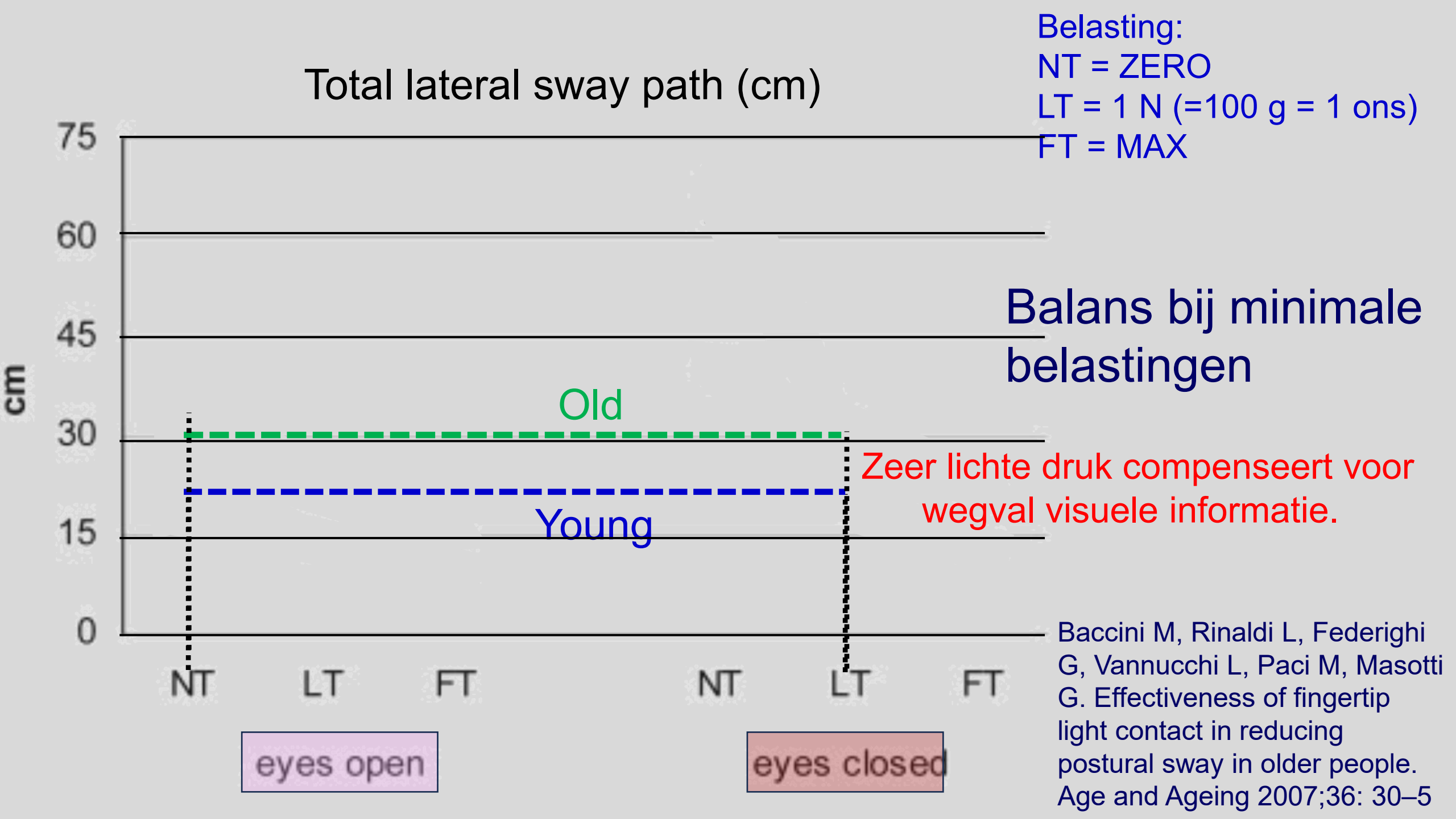


Zeer lichte druk compenseert voor
wegval visuele informatie.

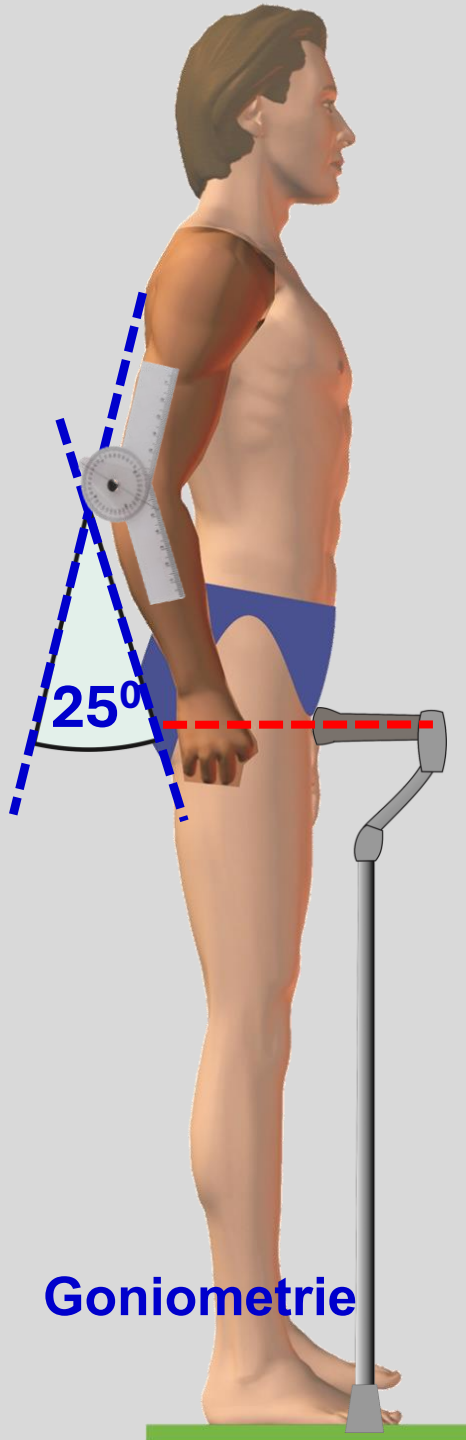


Balans bij minimale belastingen.

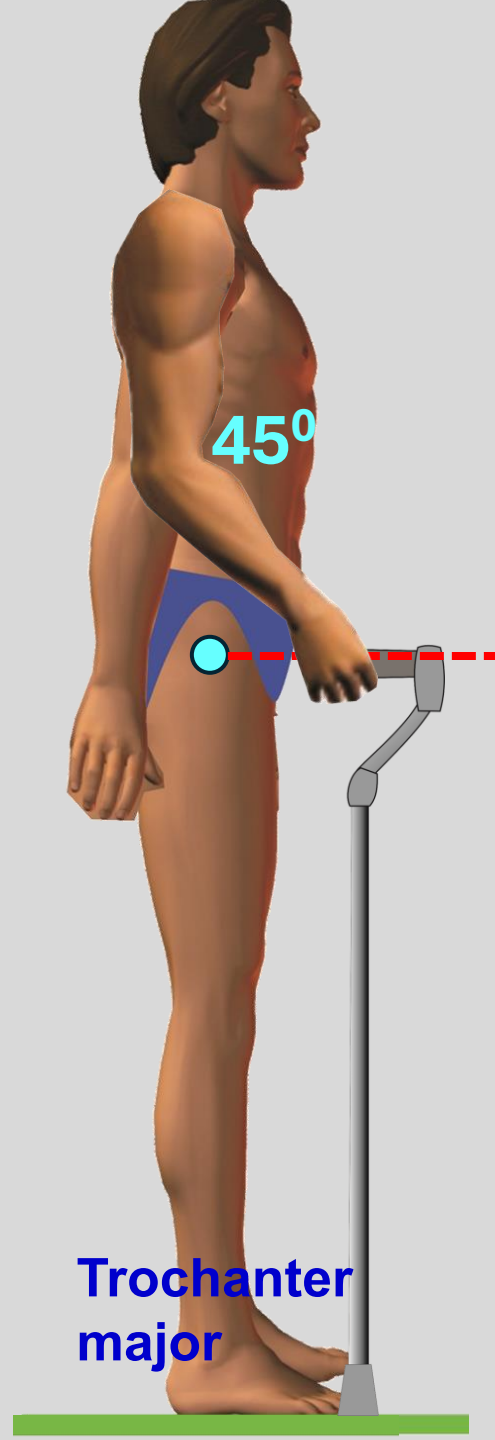
Jeka J. Light Touch Contact as a Balance
Aid. Physical Therapy 1997;77(5):476-487.



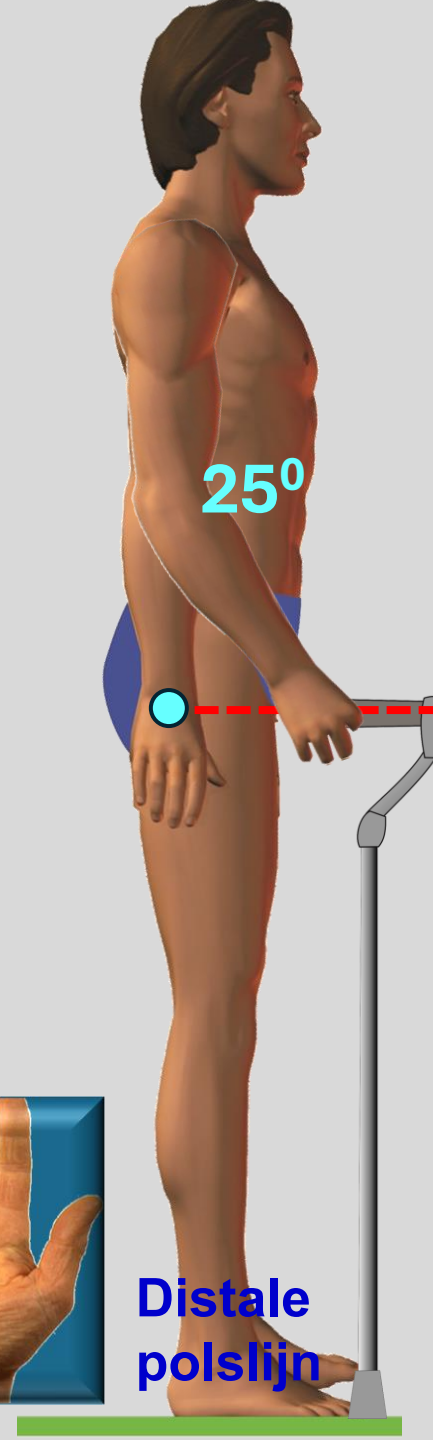
Stok lengte



Goniometrie



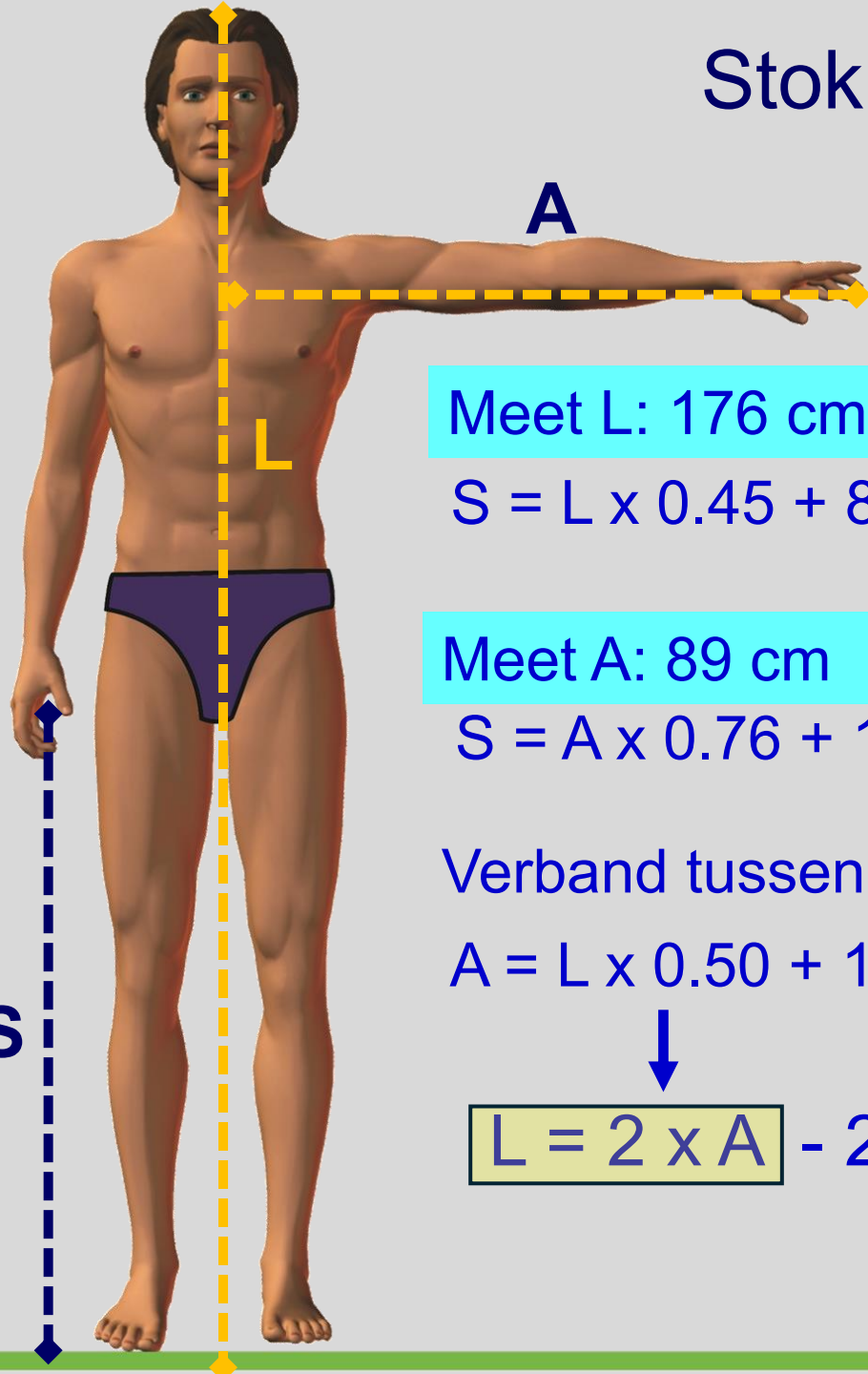
Trochanter
major



Distale
polslijn

Kumar R, Roe M, Scremin O. Methods for estimating the proper length of a cane. Arch Phys Med Rehabil 1995;76:1173-5.

Stok lengte: regressie vergelijkingen



Meet L: 176 cm

$$S = L \times 0.45 + 8.7 \text{ cm} \quad \left. \vphantom{S = L \times 0.45 + 8.7 \text{ cm}} \right\} S = 88 \text{ cm}$$

Meet A: 89 cm

$$S = A \times 0.76 + 19 \text{ cm} \quad \left. \vphantom{S = A \times 0.76 + 19 \text{ cm}} \right\} S = 87 \text{ cm}$$

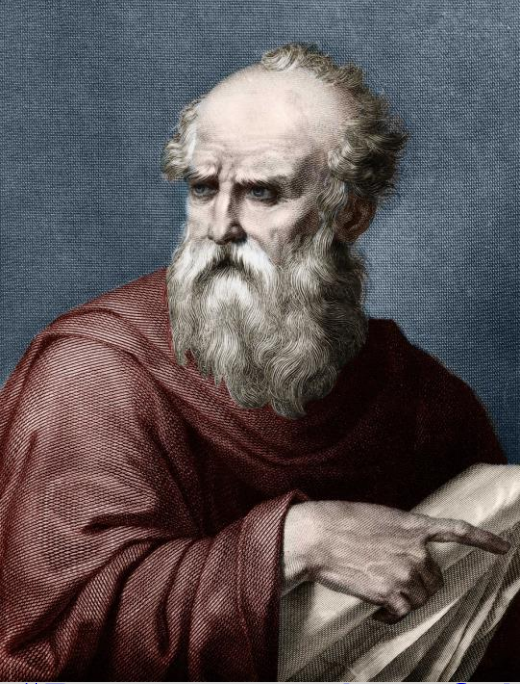
Verband tussen L en A

$$A = L \times 0.50 + 1 \text{ cm}$$



$$\boxed{L = 2 \times A} - 2 \text{ cm}$$

Kumar R, Roe M, Scremin O.
Methods for estimating the proper
length of a cane. Arch Phys Med
Rehabil 1995;76:1173-5.



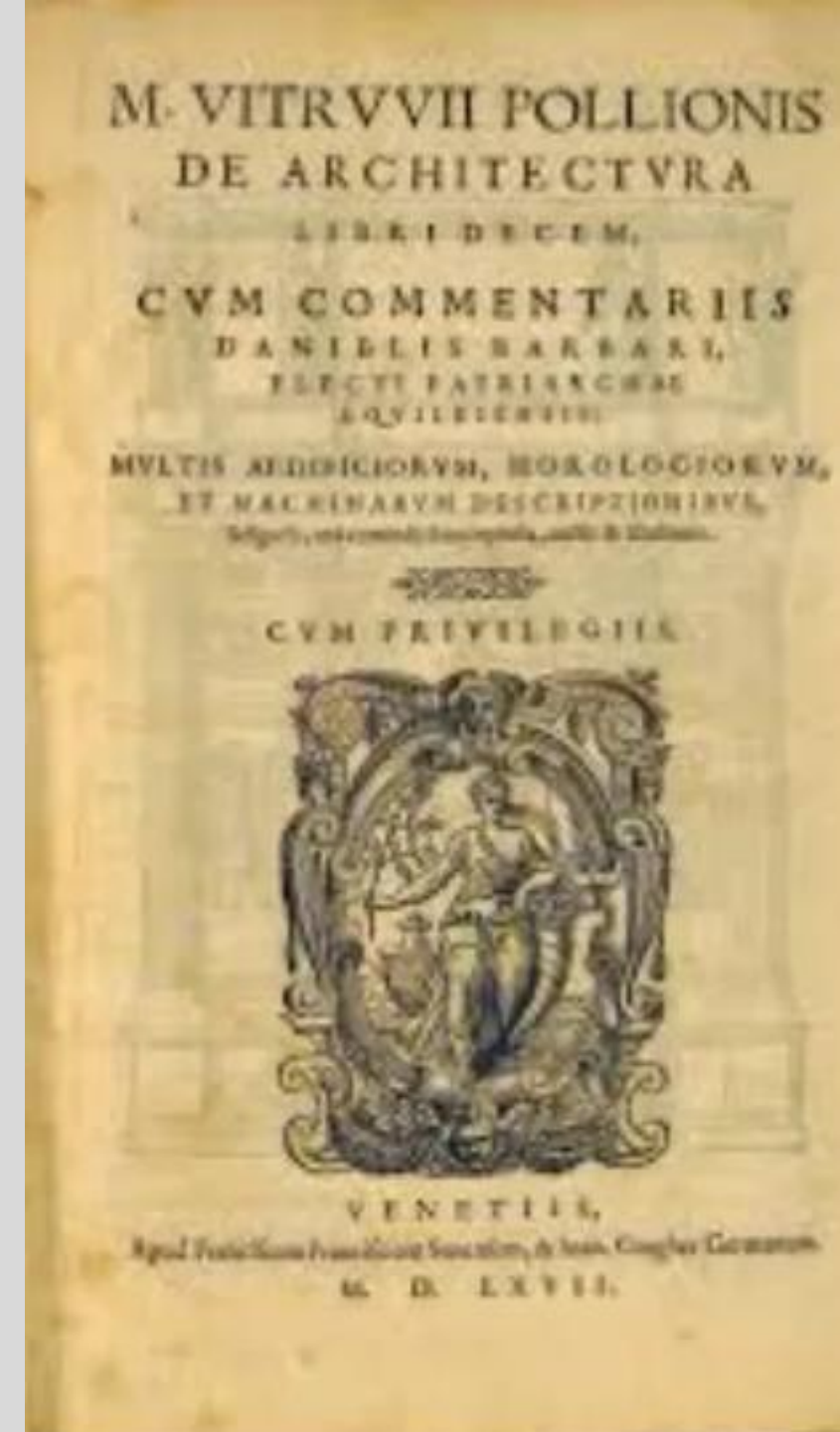
Marcus Vitruvius Pollio

Architect

85 – 20 v. Chr

De Architectura

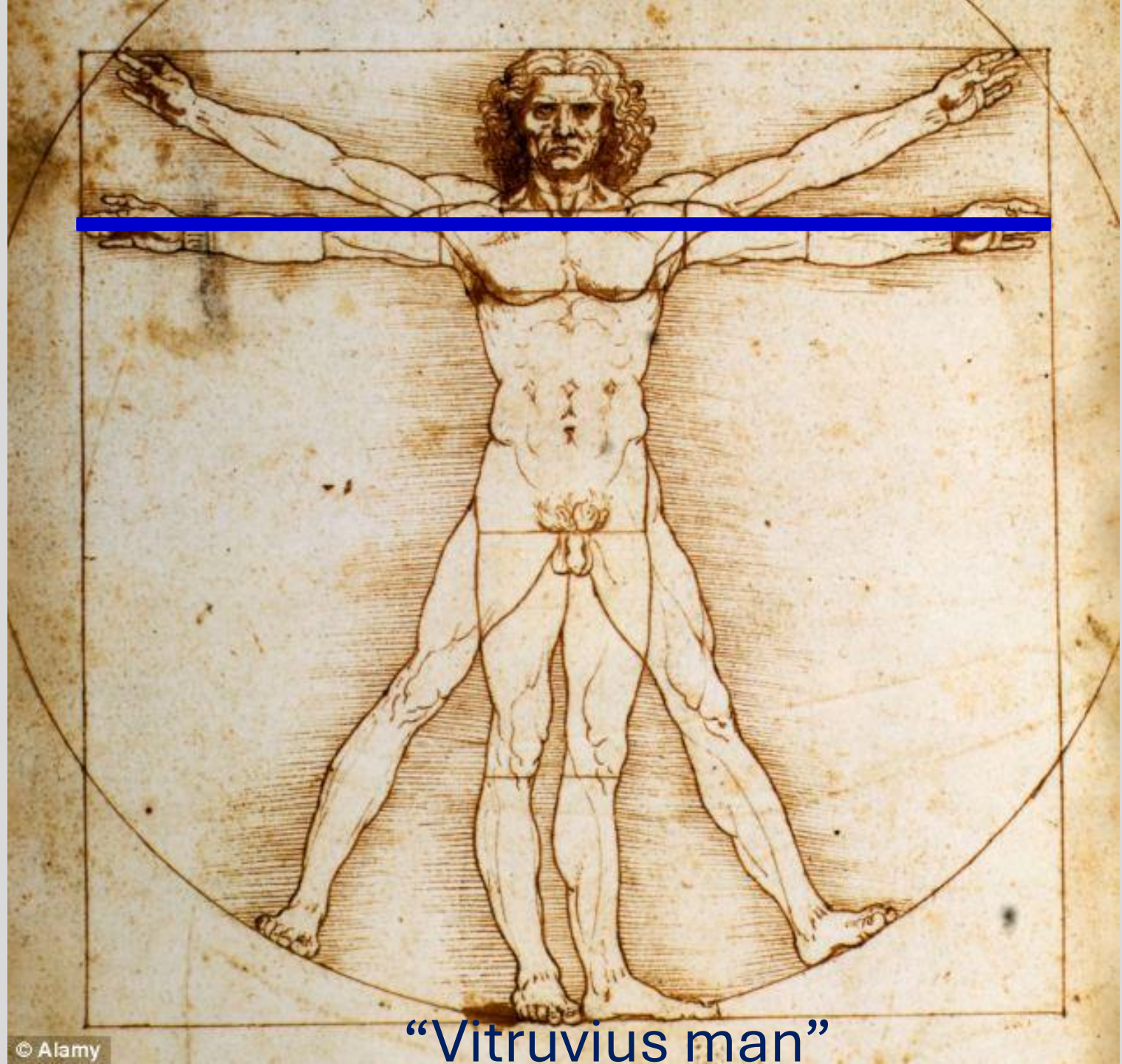
- “De natuur heeft het menselijk lichaam zo gevormd dat:
- een open gespreide armspanwijdte gelijk is aan de lichaamslengte;
 - het hoofd een achtste van de totale lichaamslengte is;
 - het gezicht een tiende van de lengte is;
 - de voet een zesde is van de lengte van het lichaam;
 - de onderarm (van elleboog tot hand) een vierde is;
 - de handpalm een tiende is;
 - en zo verder.”



Leonardo da Vinci
1452-1519



1490

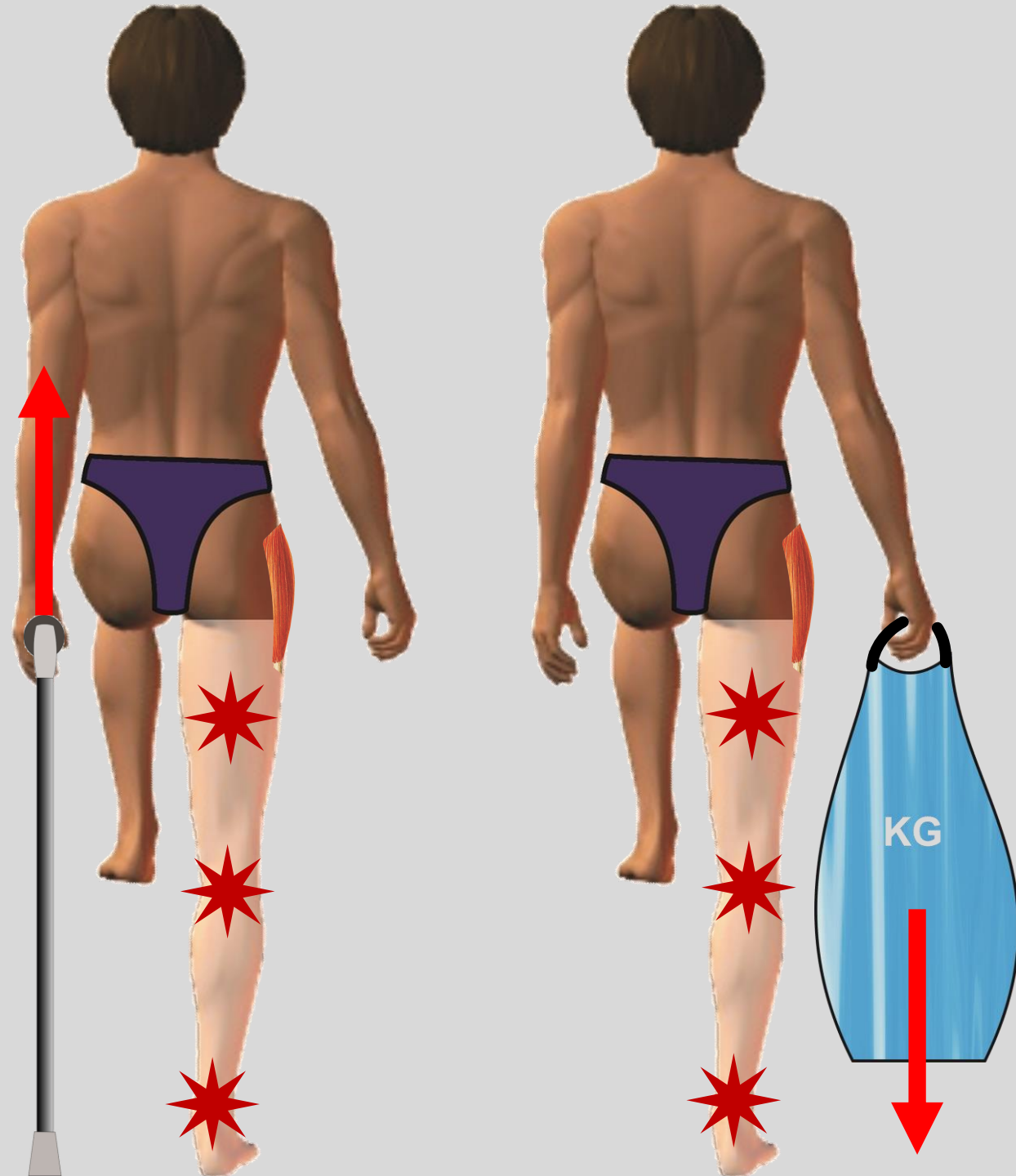


“Vitruvius man”

Om te onthouden:

Een stok altijd gebruiken aan de *gezonde* zijde.

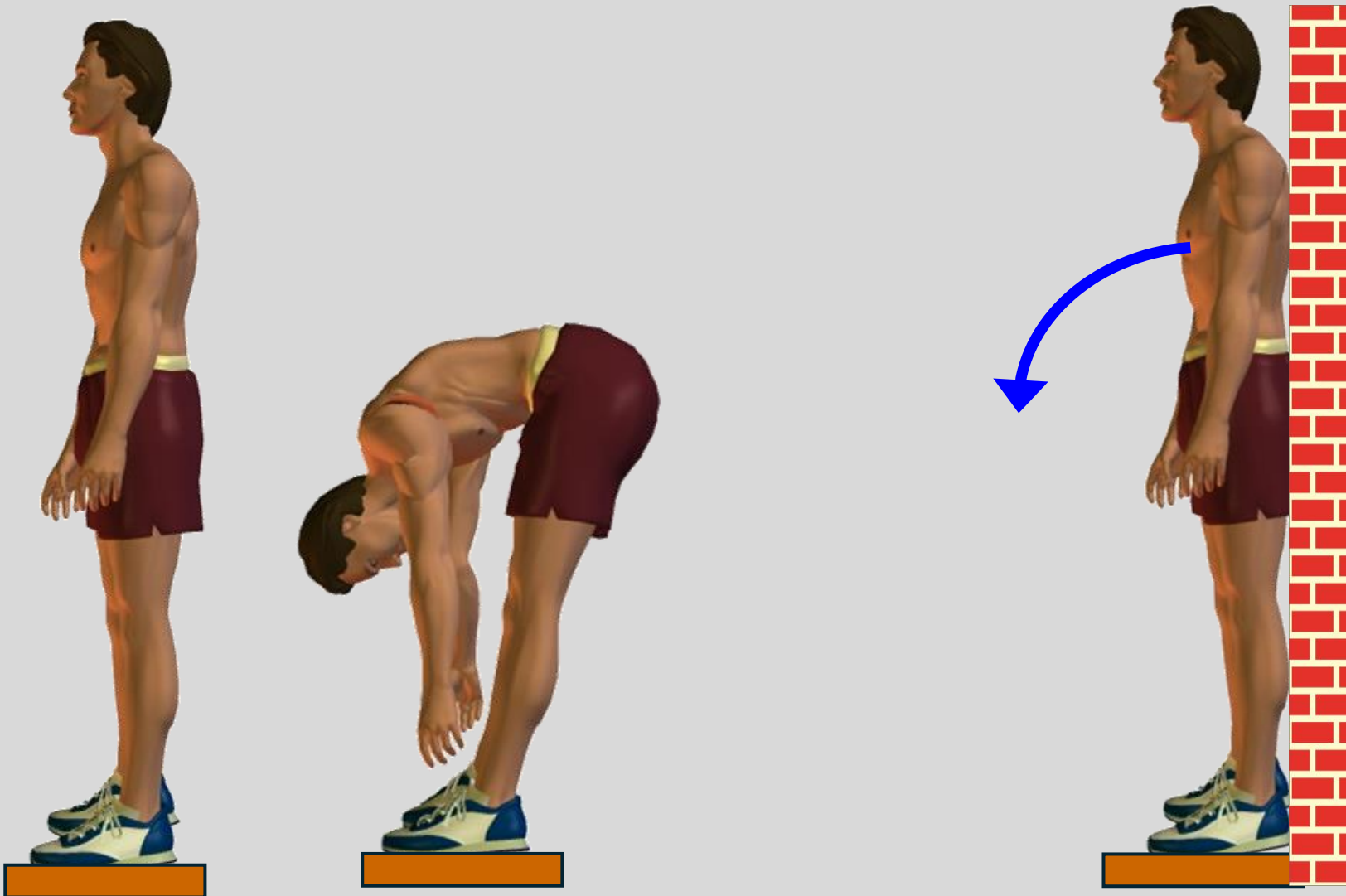
Bij verzwakte heupabductoren (Duchenne en Trendelenburg) moet een last aan de *aangedane* zijde worden gedragen.



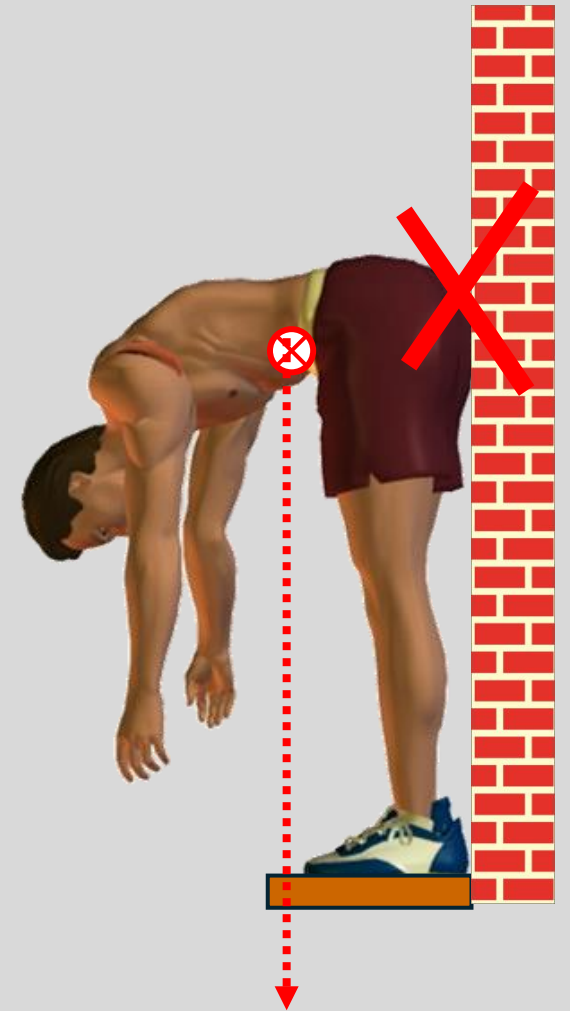
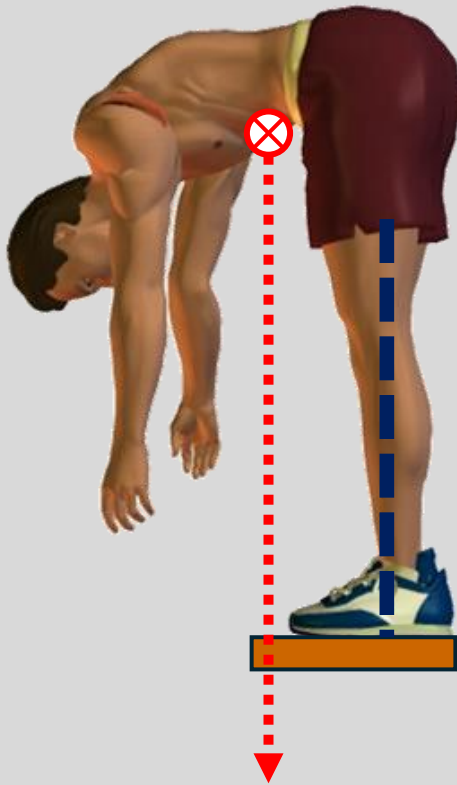
Dank voor uw aandacht



Zwaartepunt en Steunvlak 1



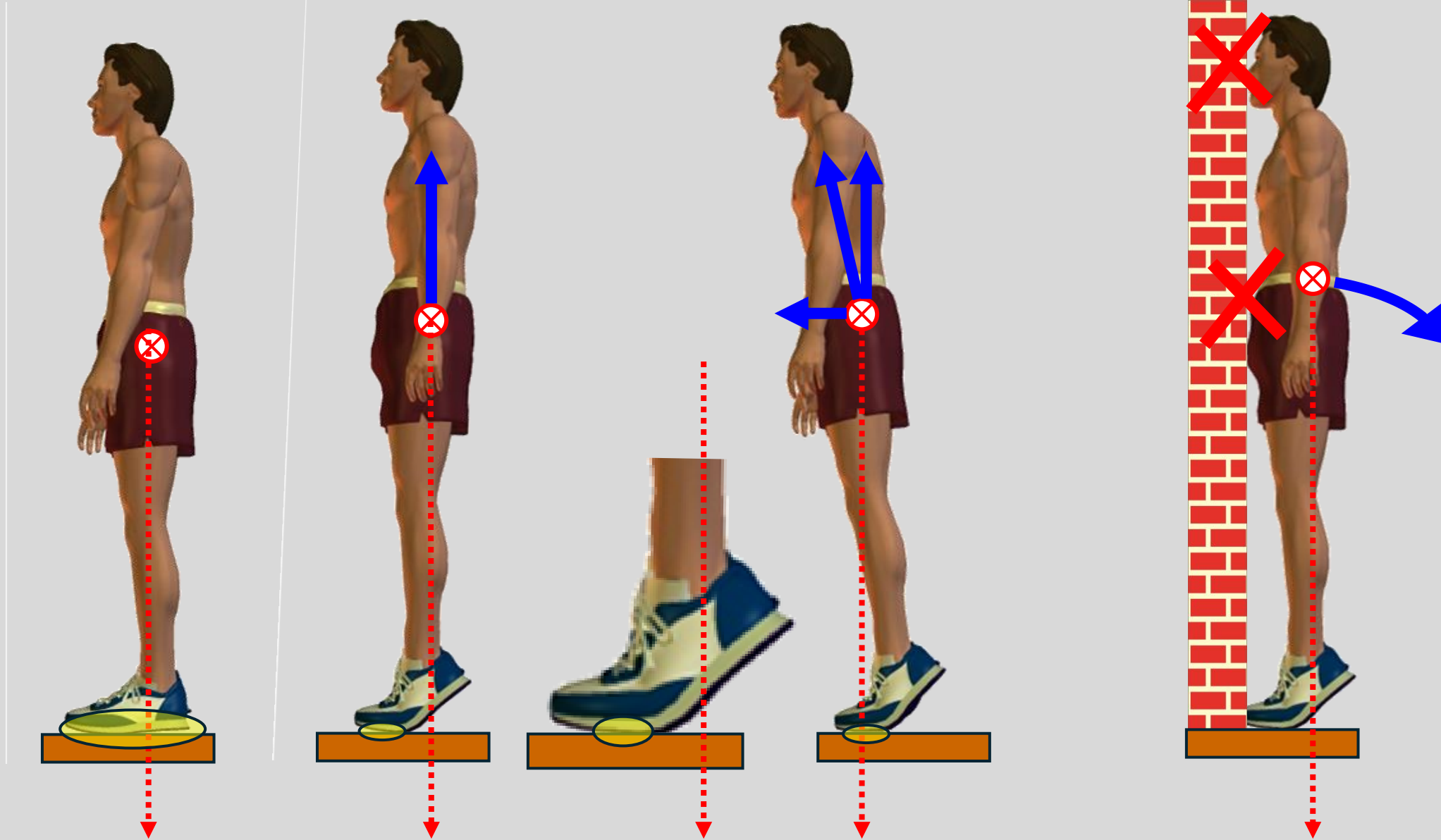
Zwaartepunt en Steunvlak 1: verklaring



Zwaartepunt en Steunvlak 2



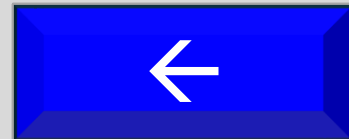
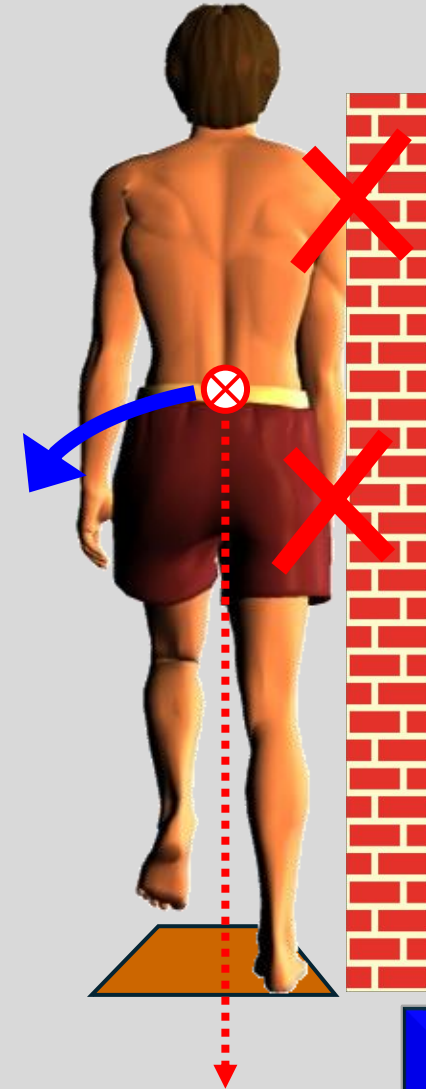
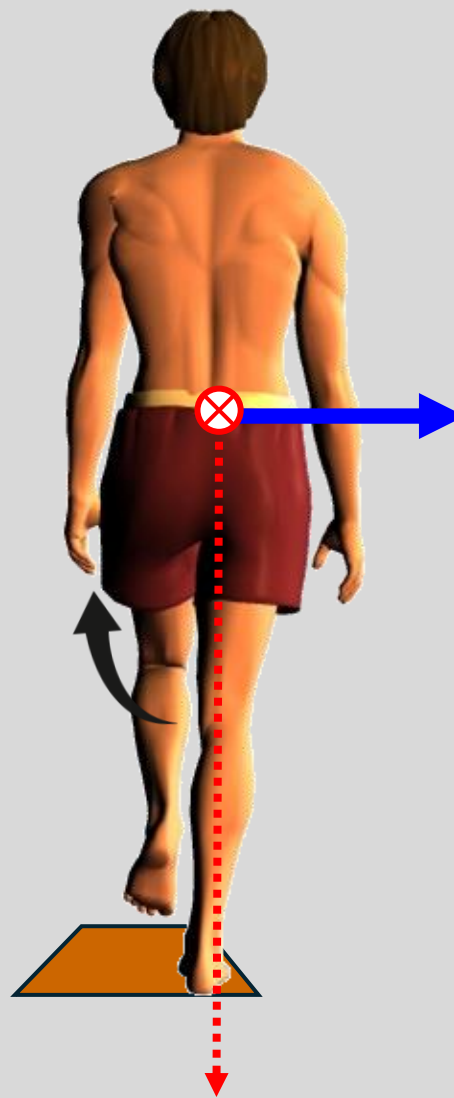
Zwaartepunt en Steunvlak 2: verklaring



Zwaartepunt en Steunvlak 3



Zwaartepunt en Steunvlak 3: verklaring





Fys.doorsnede: 12 cm²

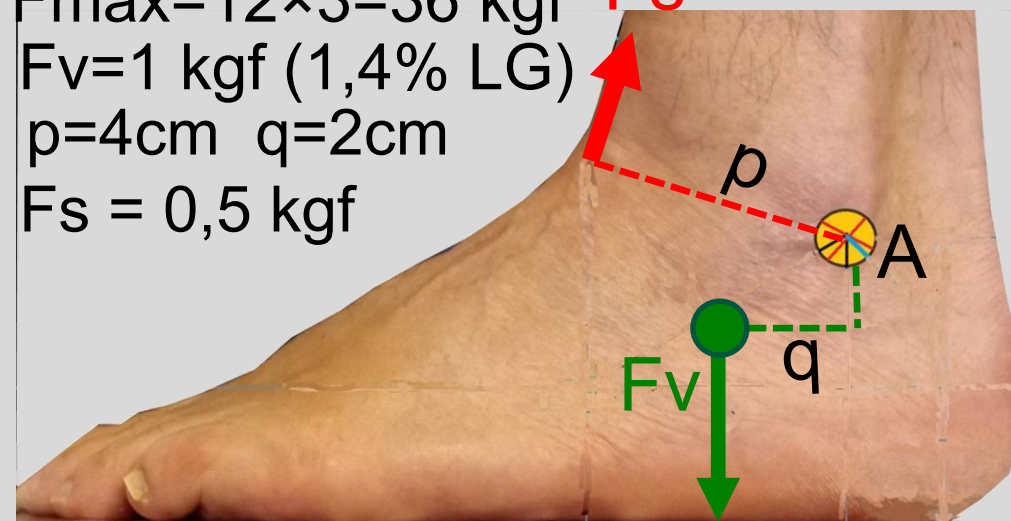
Fspecifiek: 3 kgf/cm²

Fmax=12×3=36 kgf

Fv=1 kgf (1,4% LG)

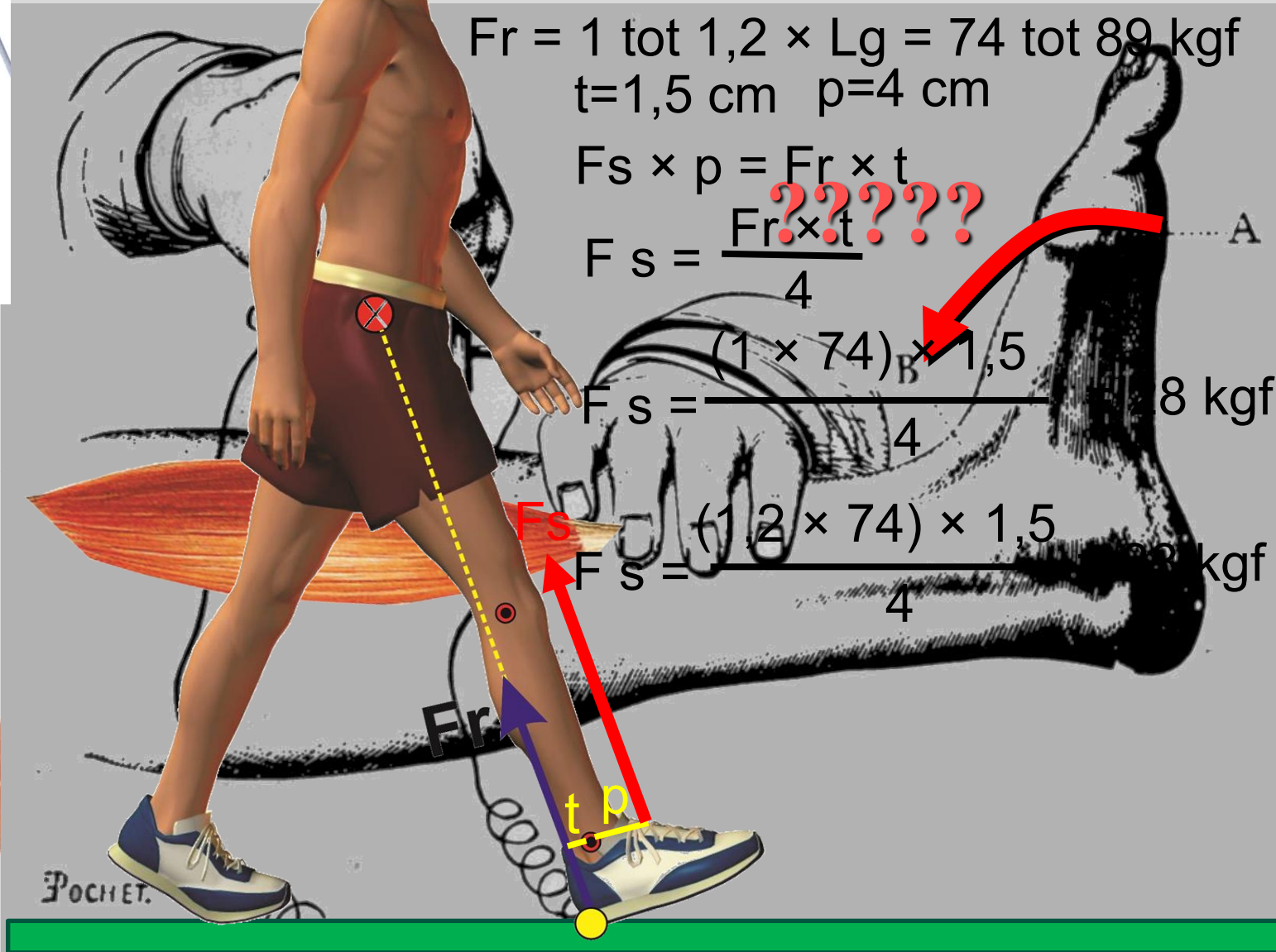
p=4cm q=2cm

Fs = 0,5 kgf

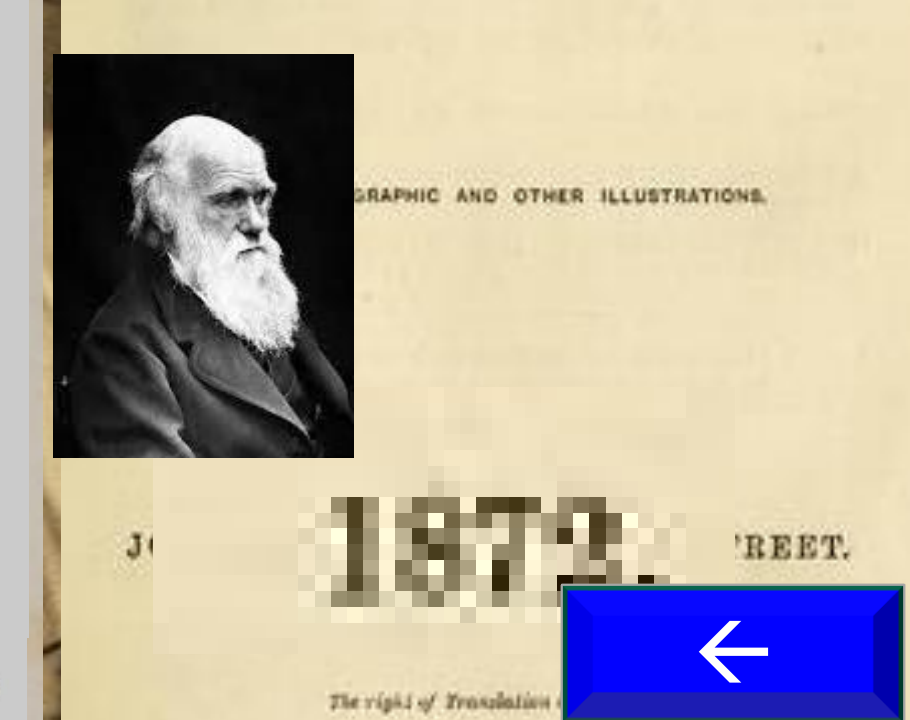
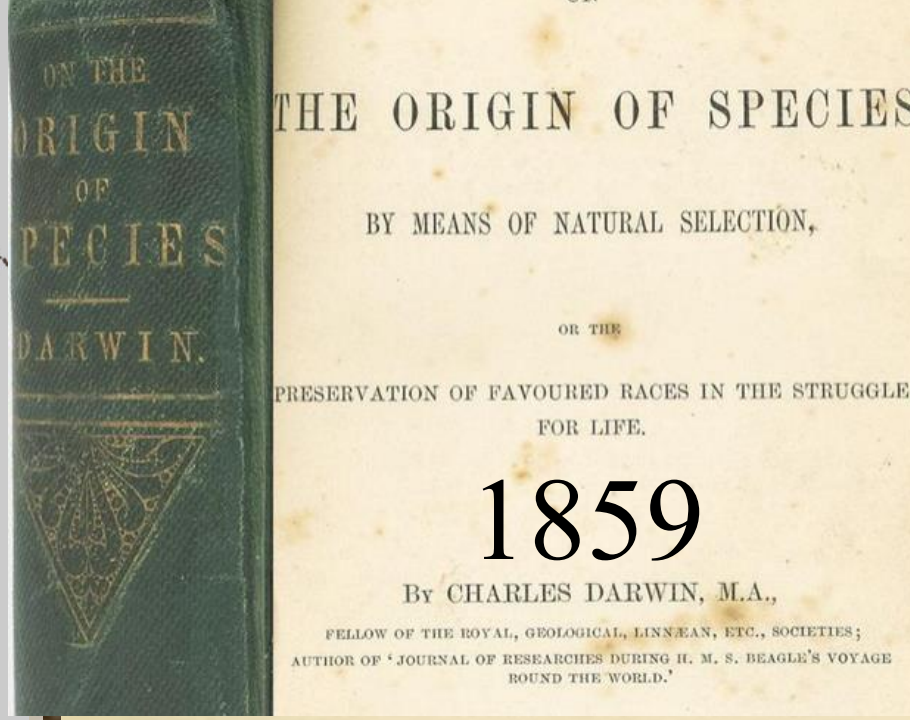
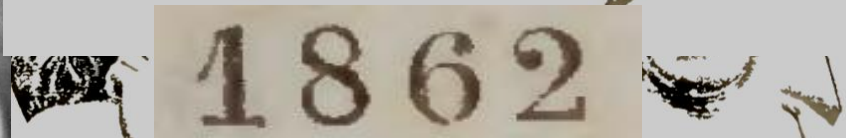
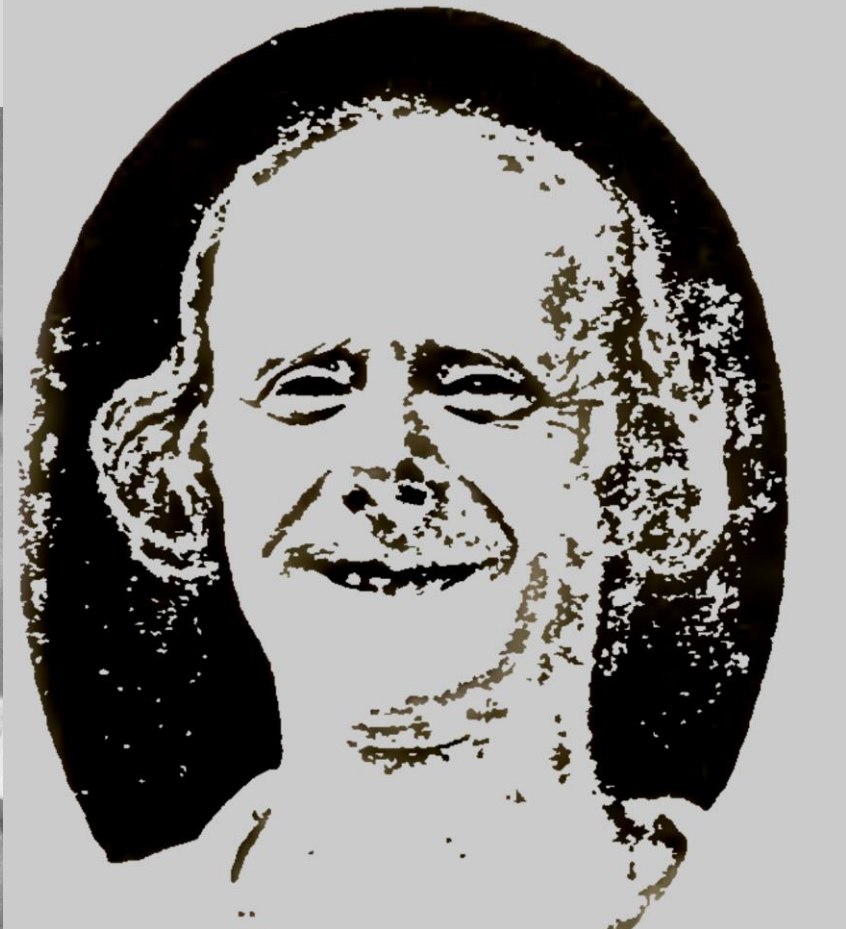
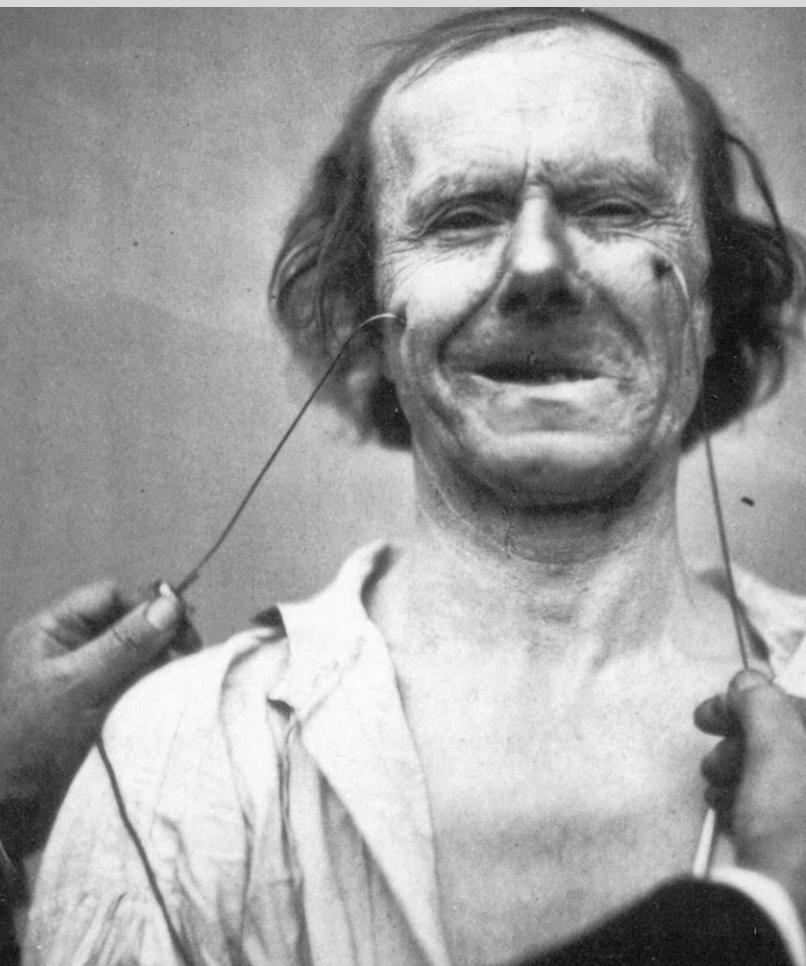


Fmax is 72 × groter dan Fv

Physiologie des mouvements

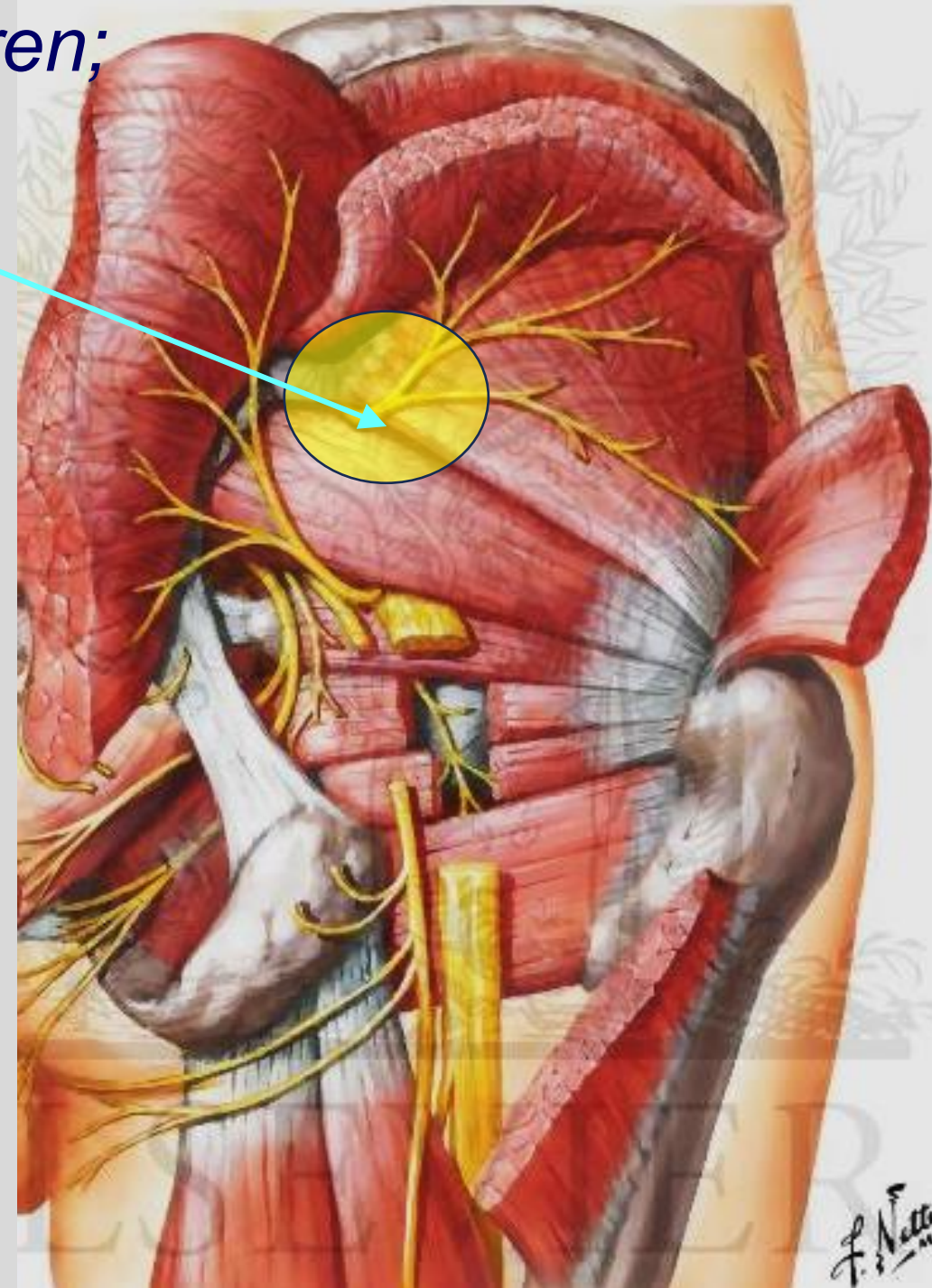
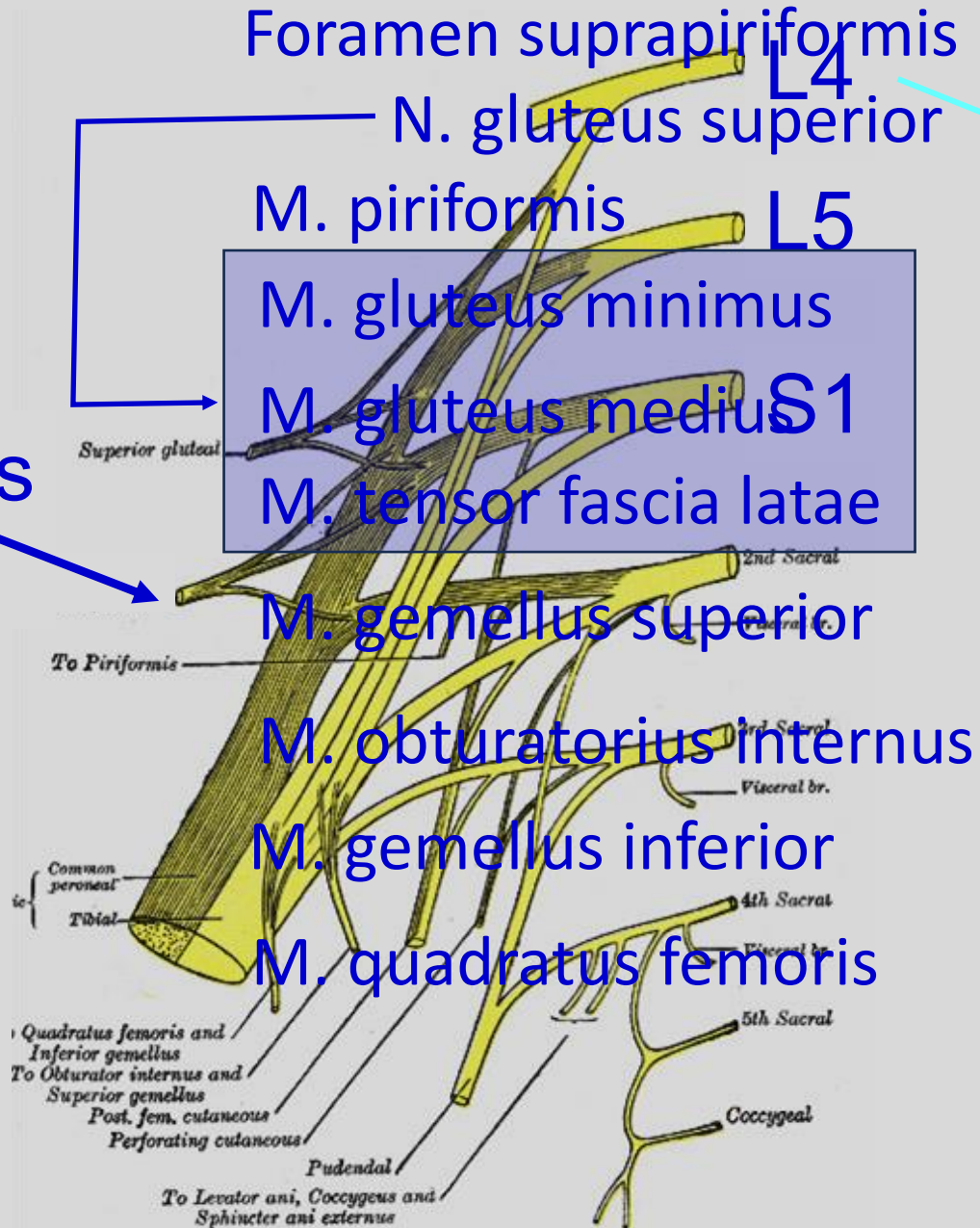


**Guillaume-Benjamin
Duchenne de Boulogne
1806-1875 Mécanisme de la
physionomie humaine ou
analyse électrophysiologique de
l'expression des passions.**

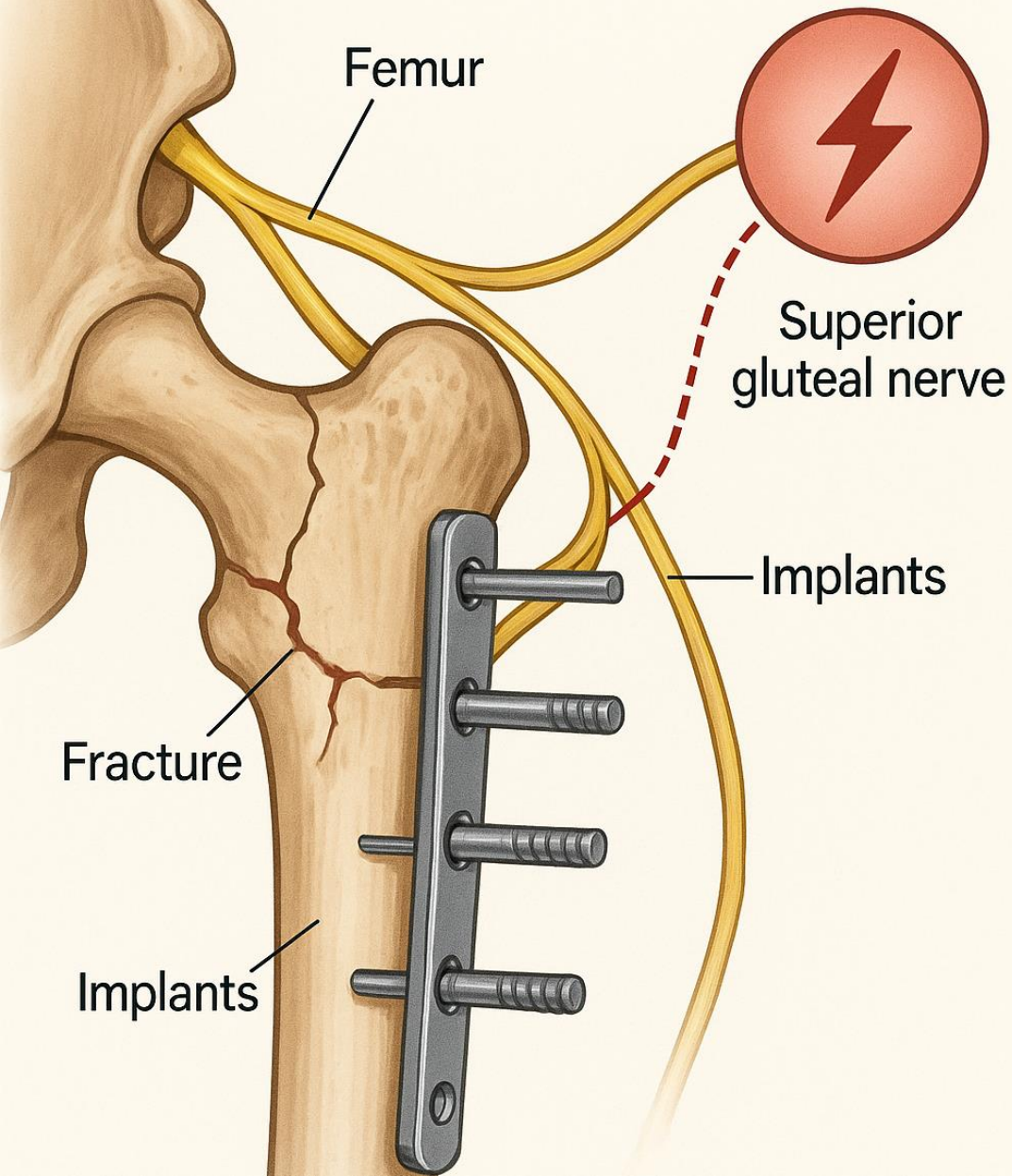


- *parese/paralyse van de heupabductoren;*

N. gluteus superior



Risk of Superior Gluteal Nerve Damage



Vraag het AI:

Laat in één plaatje zien hoe het inbrengen van pennen, platen en schroeven in het femur bij een fractuur, kan leiden tot een beschadiging van de N. gluteus superior

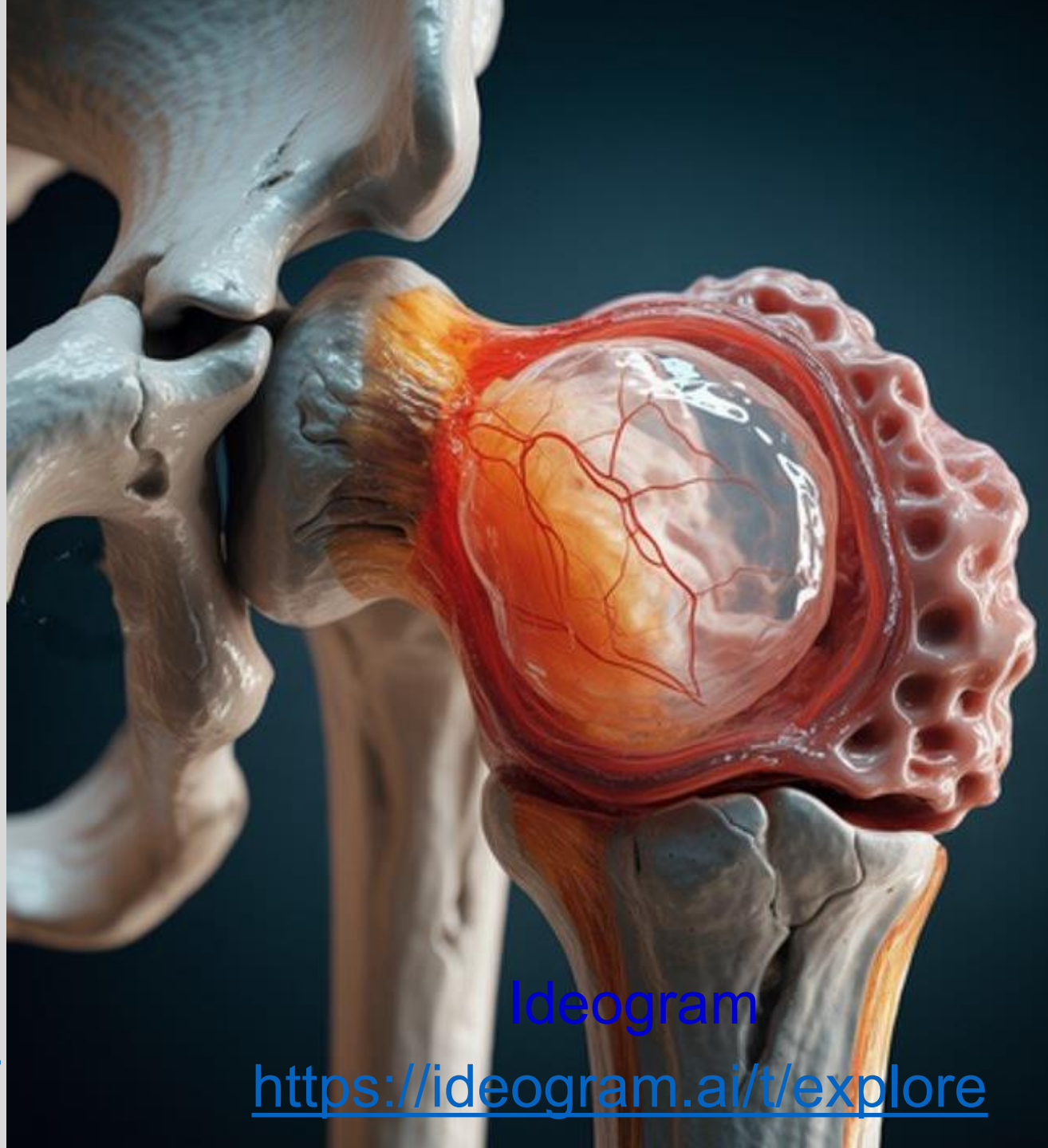
Perplexity

<https://www.perplexity.ai/search/laat-in-1-plaatje-zien-hoe-het-bgELOzUbTKGOX4mEa2ERkg>



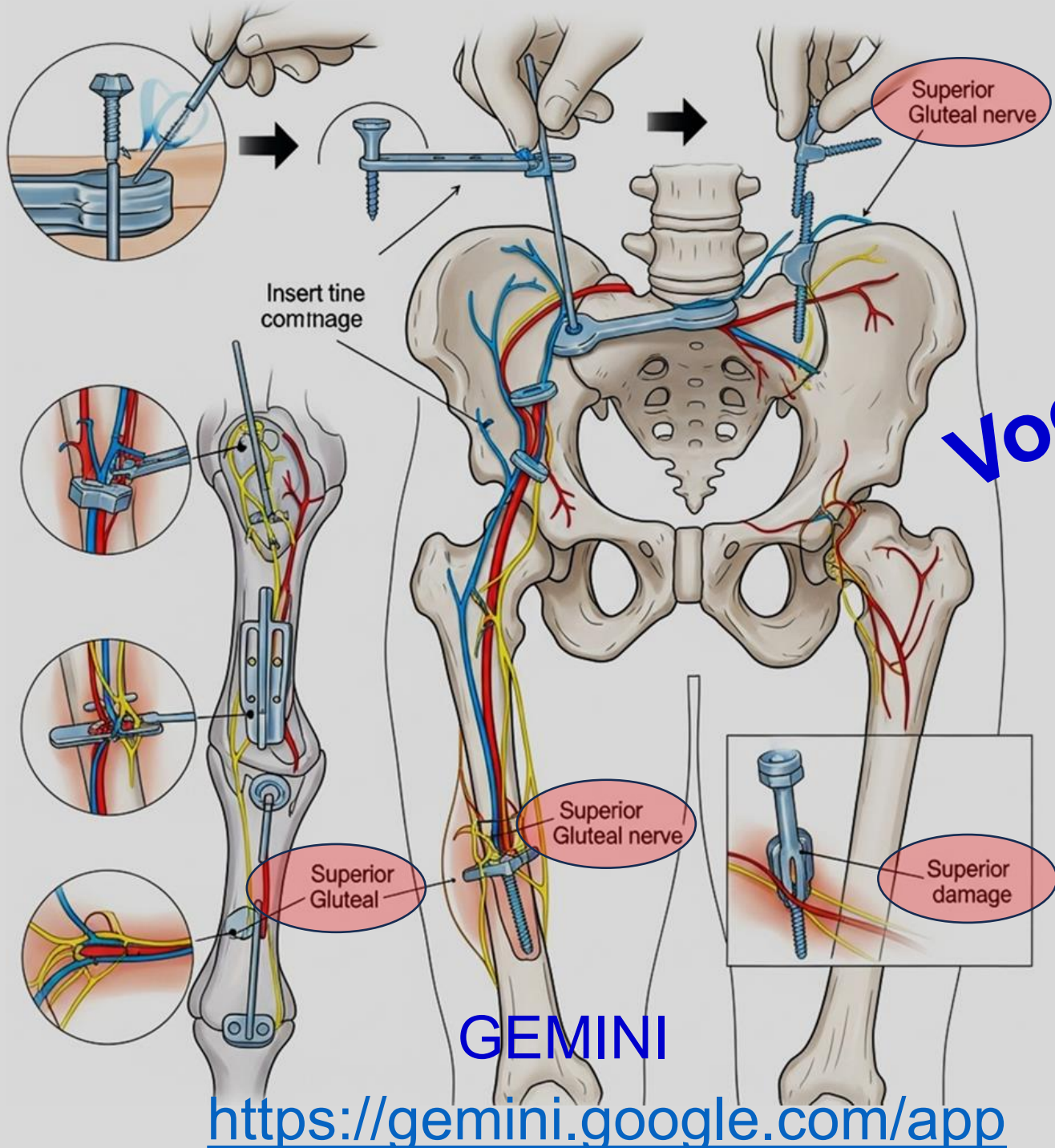
AI Image Generator

<https://deepai.org/machine-learning-model/text2img>

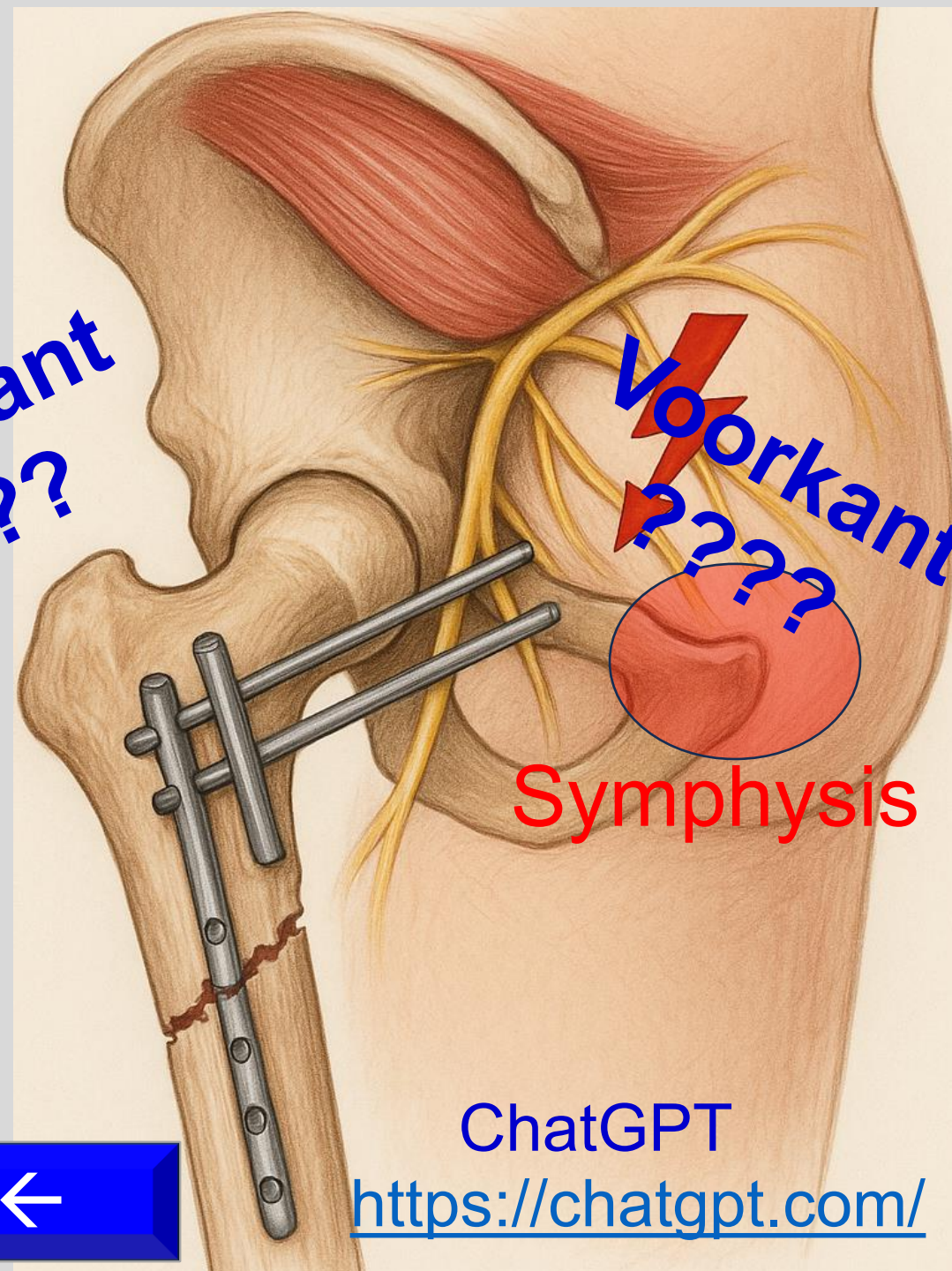


Ideogram

<https://ideogram.ai/t/explore>



Voorkant
?????



Voorkant
?????

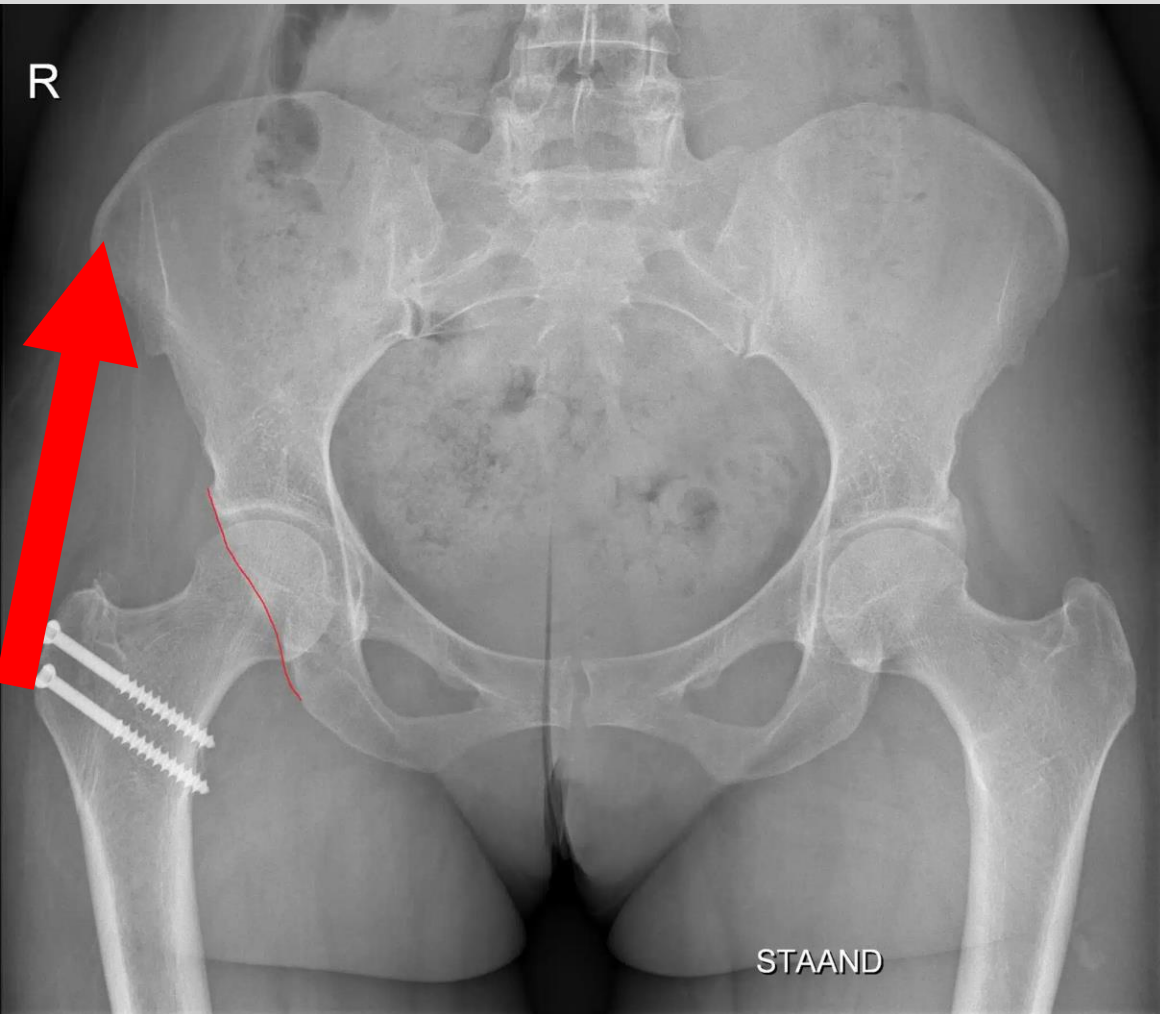
Symphysis

ChatGPT

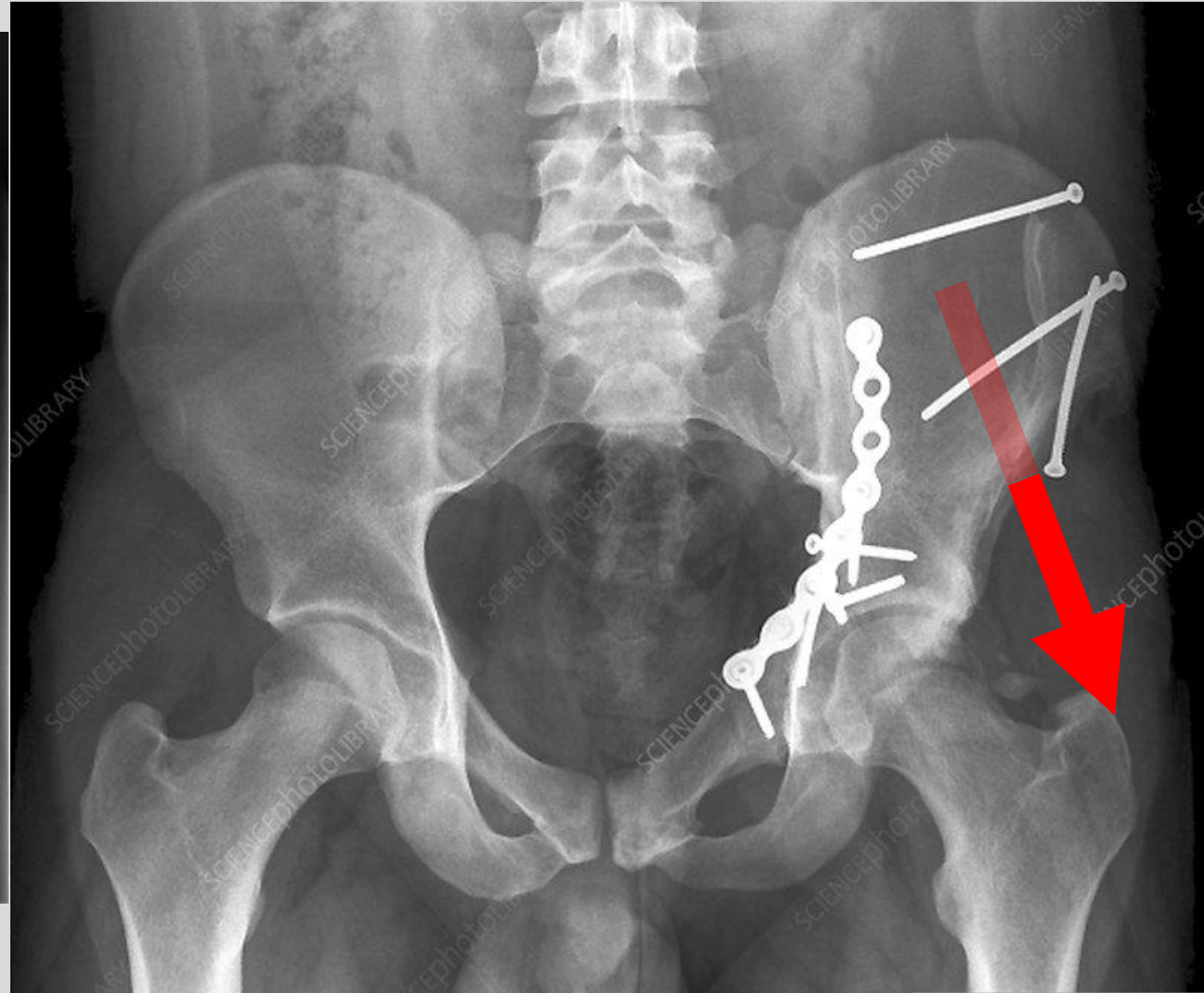
<https://chatgpt.com/>



- *beschadiging heupabductoren → contractie pijnlijk;*



<https://www.azlink.be/artikel/azlink-38/de-jonge-patient-met-heupklachten-evolutie-naar-heupsparende-chirurgie/>



<https://www.sciencephoto.com/media/90743/view/pinned-hip-fractures-x-ray>



Trueta J.
The Hip
The Hip society.
The C.V. Mosby Company (1973).

J. Trueta
Studies on the development
and decay of the human frame
William Heinemann Medical Books (1968)

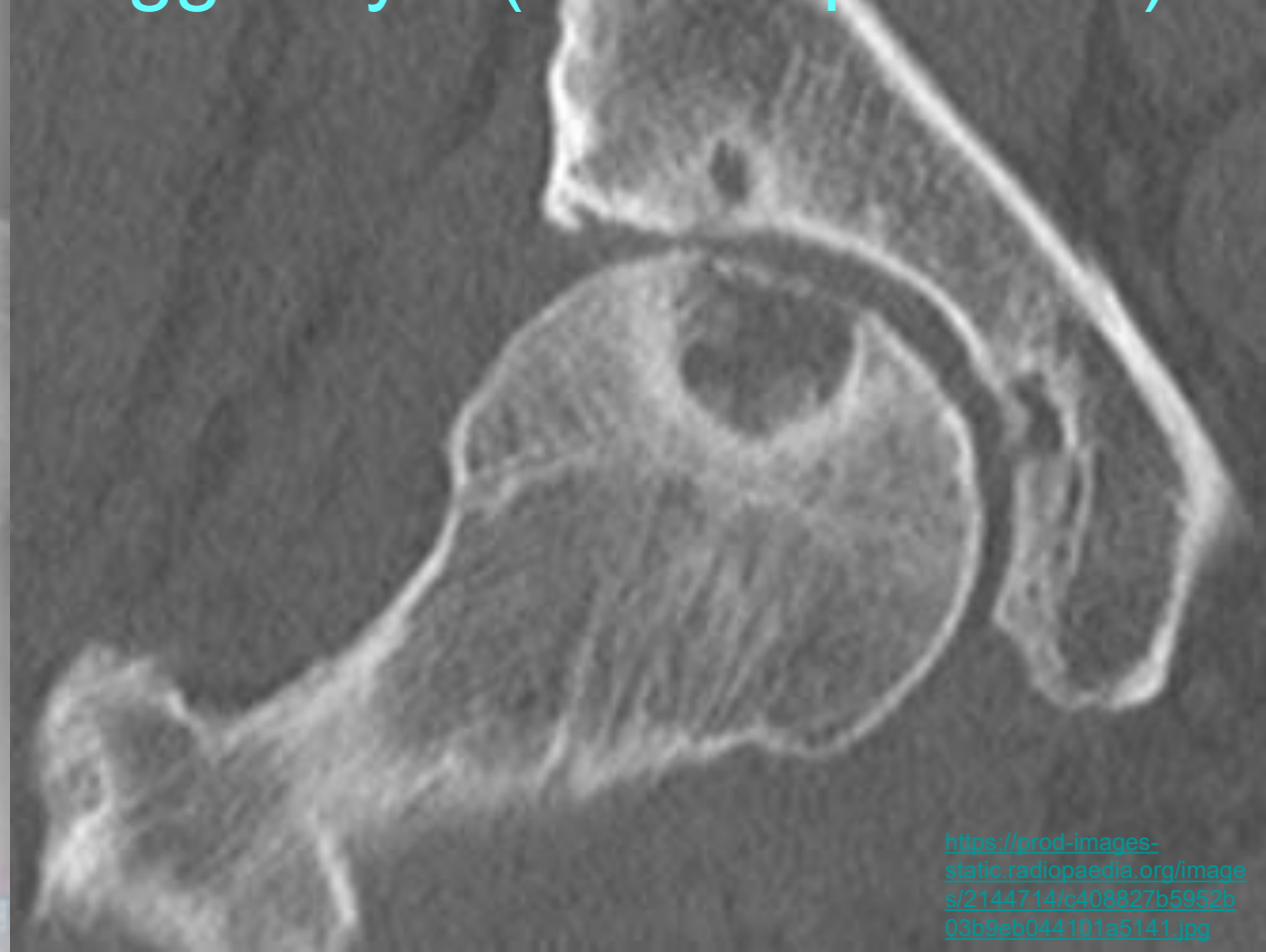
Arnoldi C. Impeded Venous Drainage from the Bone Marrow
of the Femoral Head: A Synthesis. Vascular Surgery
24(2):97-106 (1990).

Carl Arnoldi, Hakan Linderholm, Herbert Mussbichler,
Venous engorgement and intraosseous hypertension
in osteoarthritis of the hip.
The Journal Of Bone And Joint Surgery
54b, no. 3, august 1972

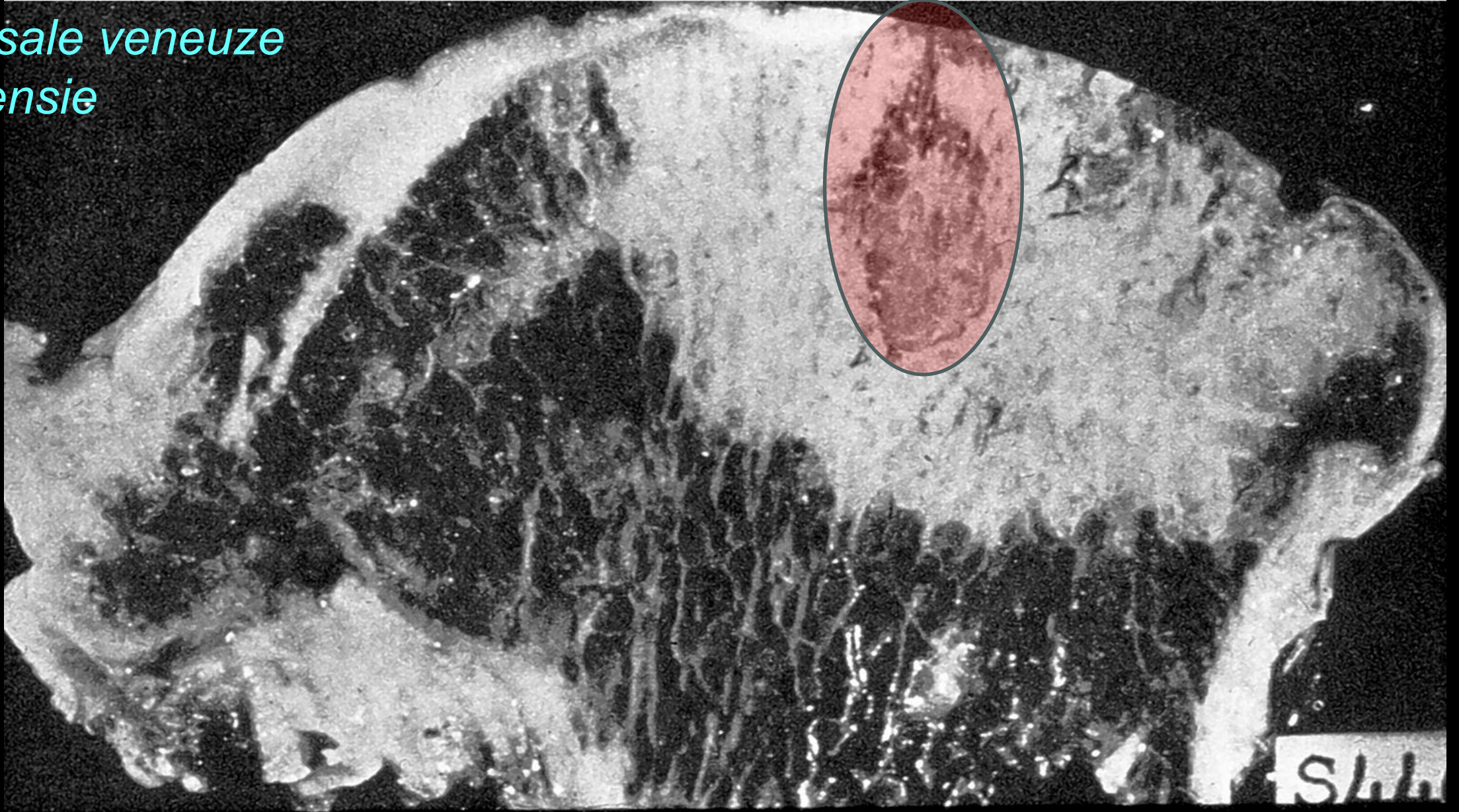
Arnoldi C. Intraosseus Hypertension
Clinical Orthopaedics and Related Research, nr.115
(1976), pp.30-34.

Subchondrale cysten en de intra- ossale veneuze hypertensie

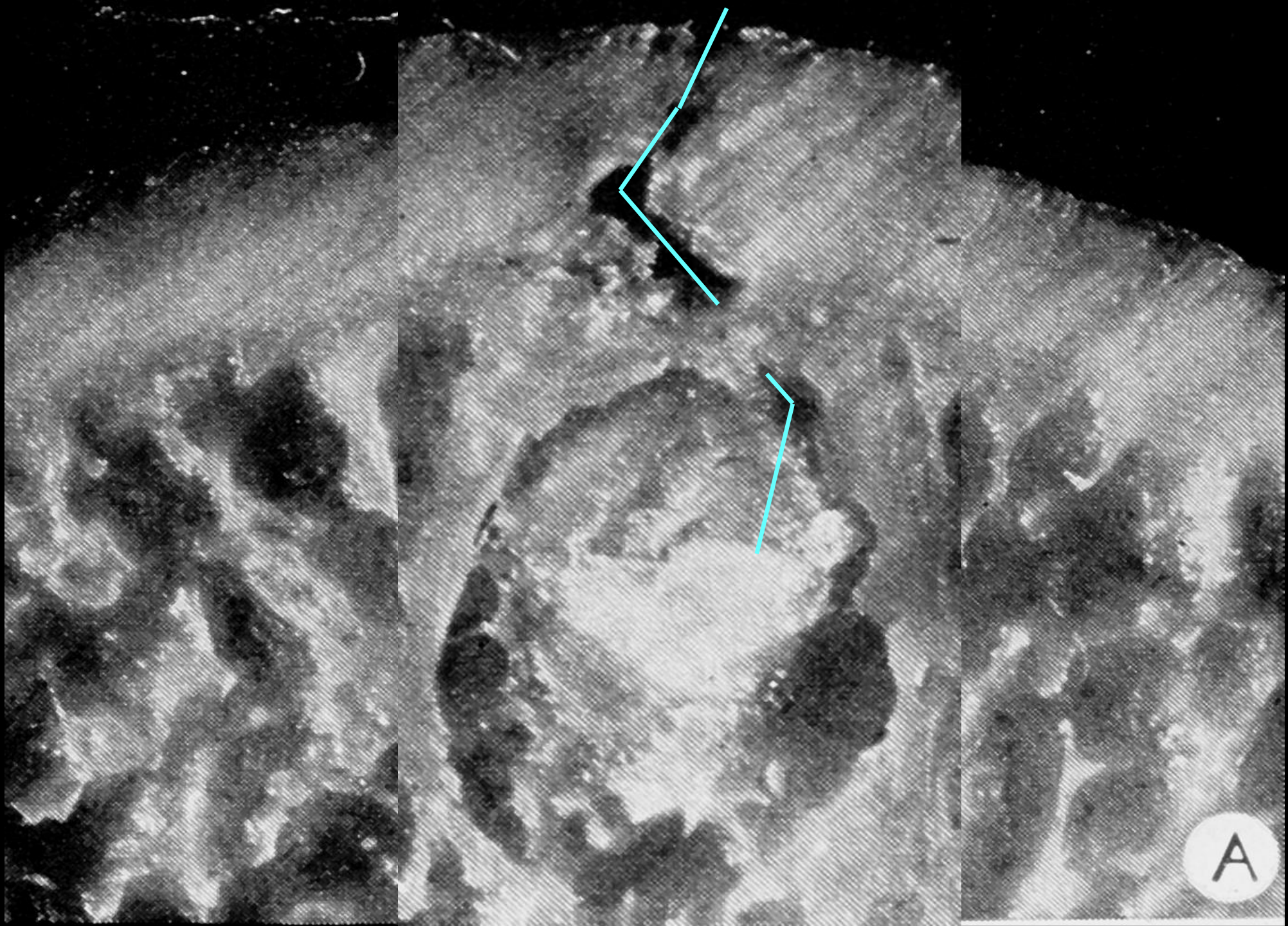
- Osteoarthritic cyst
- Pseudocyst
- Geode
- Subchondral cyst
- Egger cyst (in the hip socket)

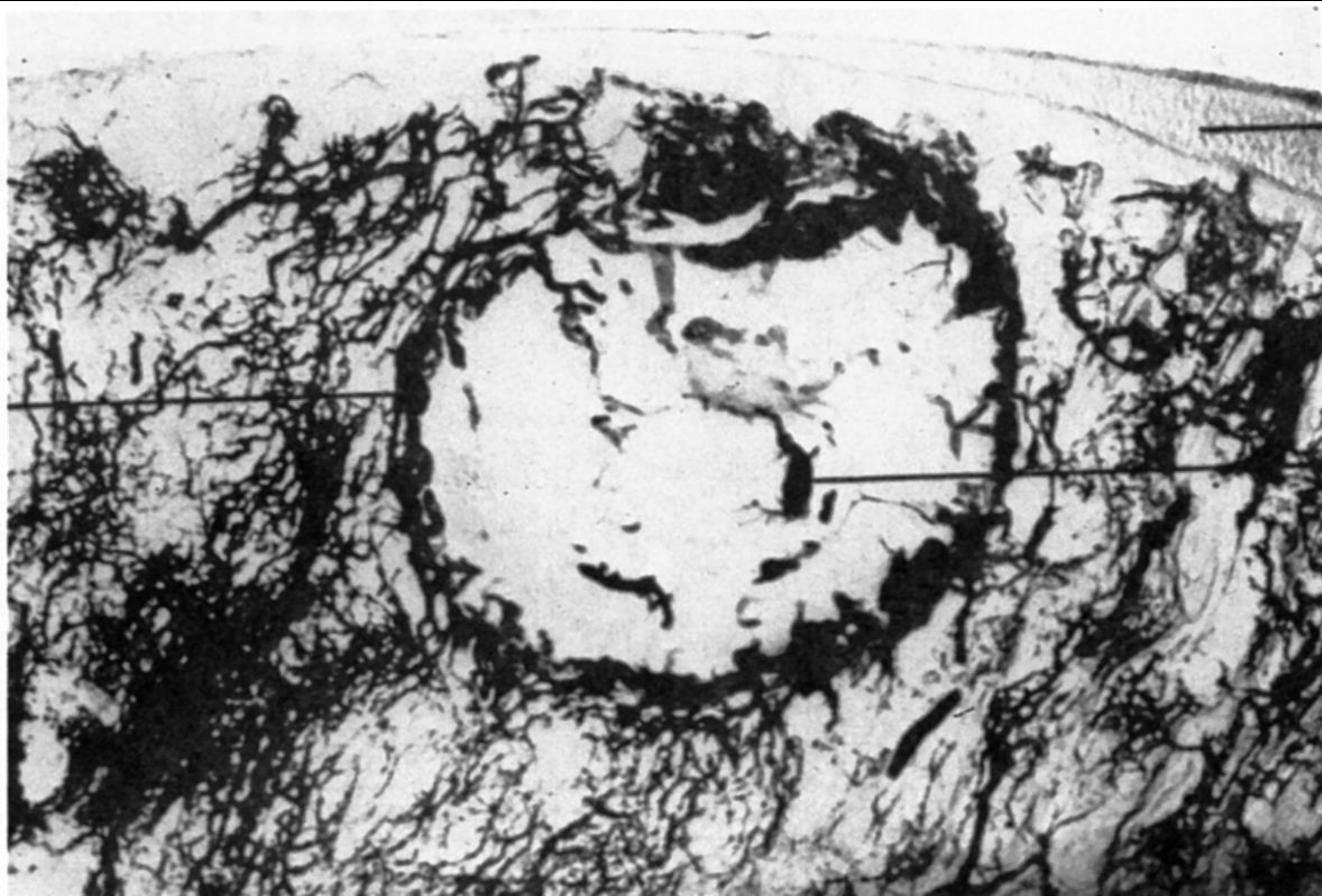


*Intraossale veneuze
hypertensie*



Naar: J. Hollander Arthritis and Allied Conditions

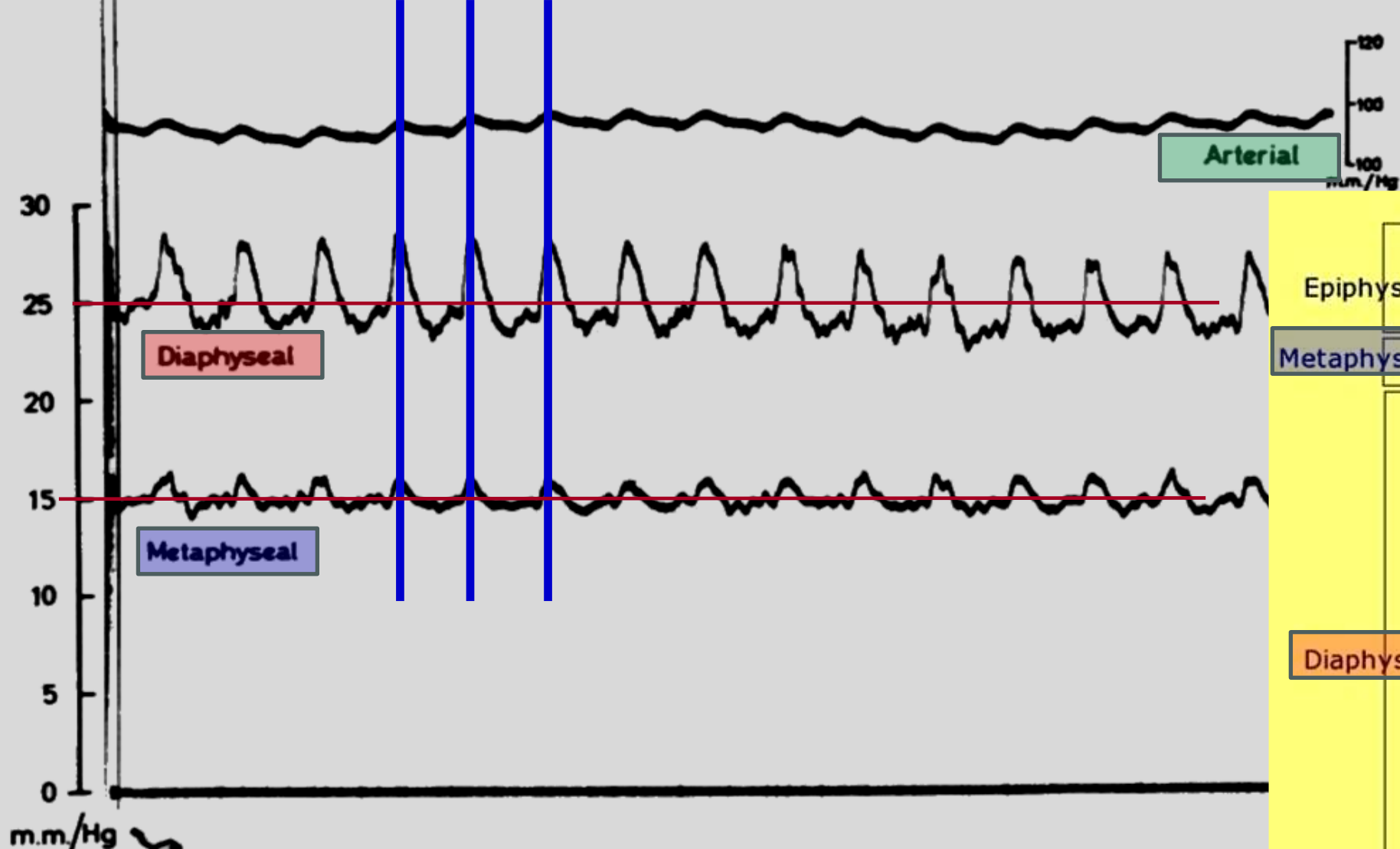




Trueta J. in:
The Hip
The Hip society.
The C.V. Mosby
Company (1973).

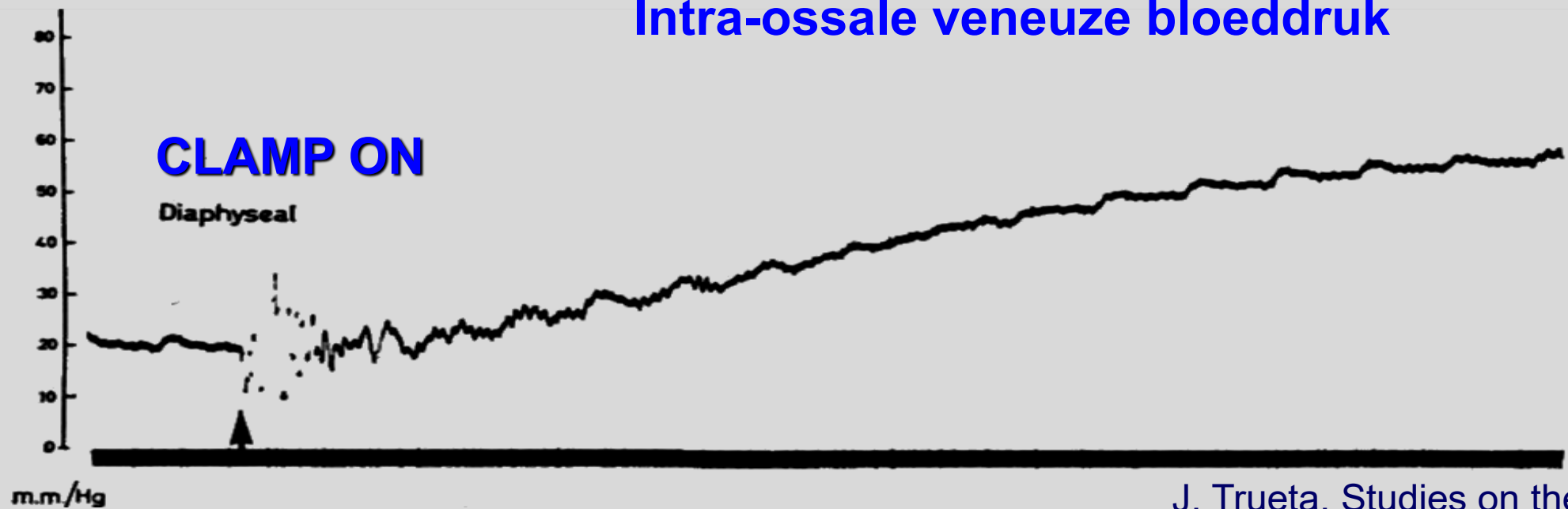
Intra-ossale
veneuze
bloeddruk

Gem. Dia- en
Meta-physe:
 $(25 + 15) / 2 =$
20 mm Hg

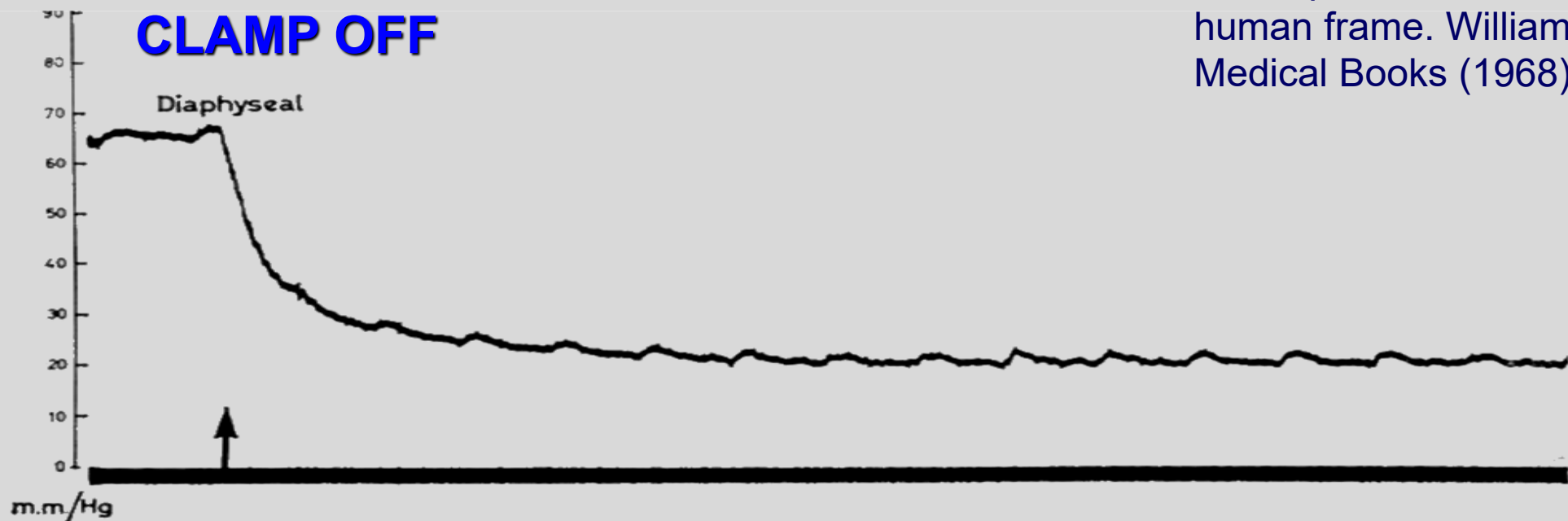


Naar J. Trueta
Studies on the development
and decay of the human frame
William Heinemann Medical Books (1968)

Intra-ossale veneuze bloeddruk

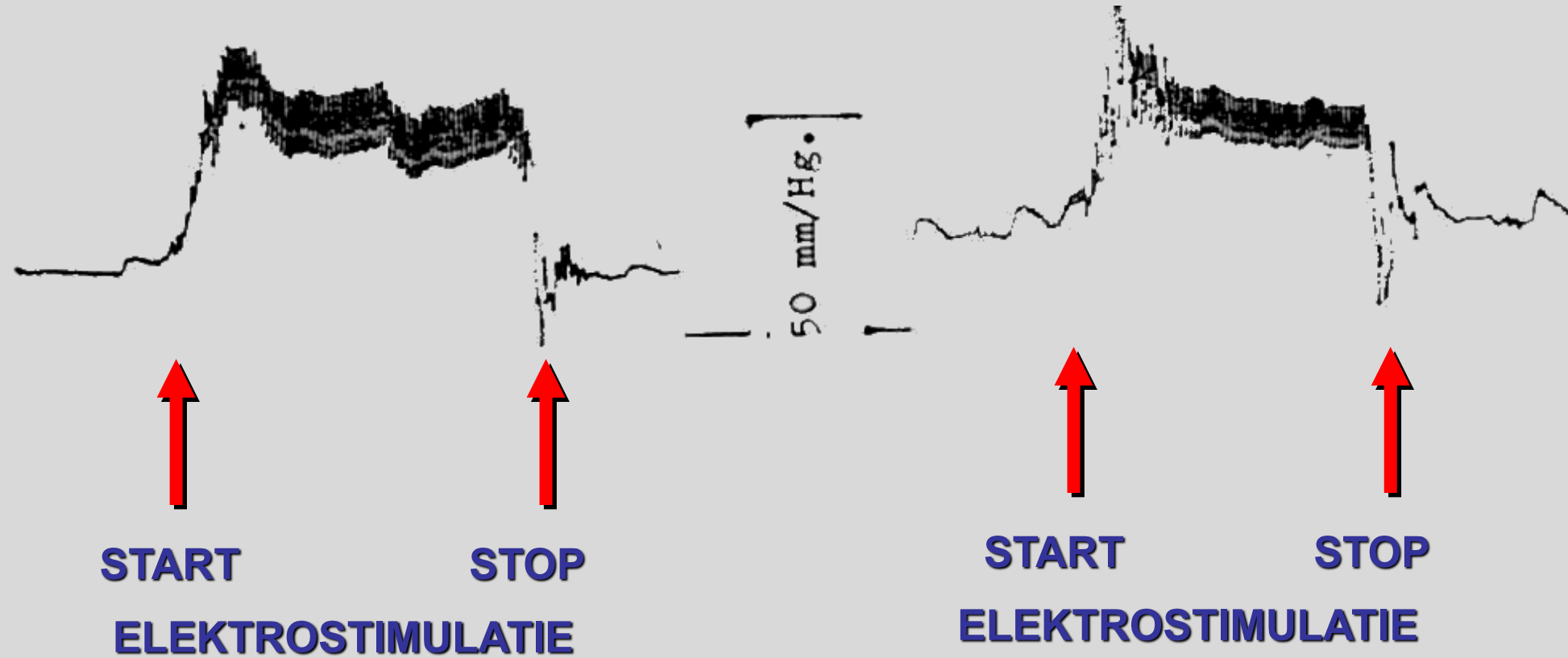


J. Trueta. Studies on the development and decay of the human frame. William Heinemann Medical Books (1968)

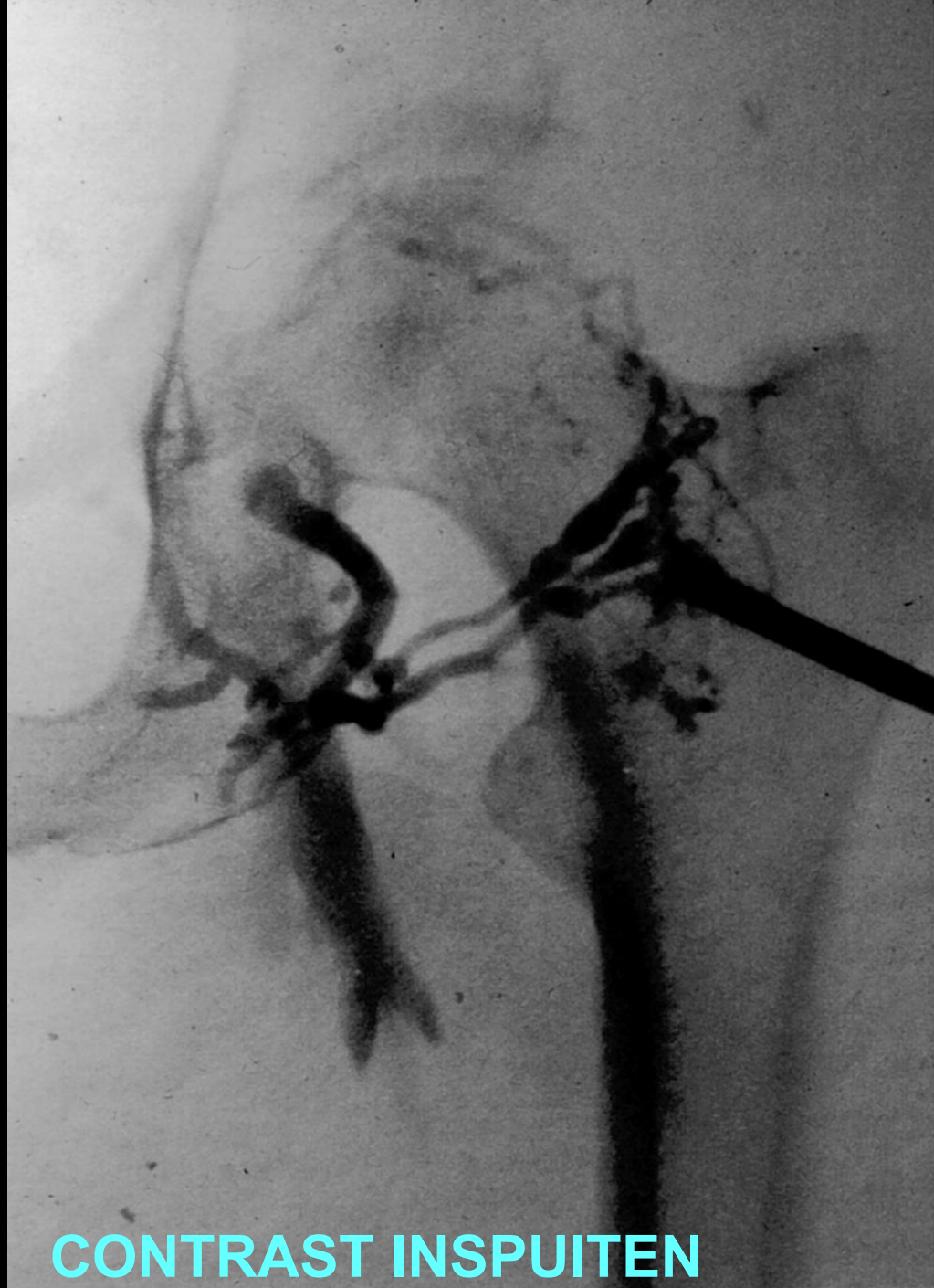


DIAFYSE

METAFYSE



J. Trueta. Studies on the development and decay of the human frame. William Heinemann Medical Books (1968)



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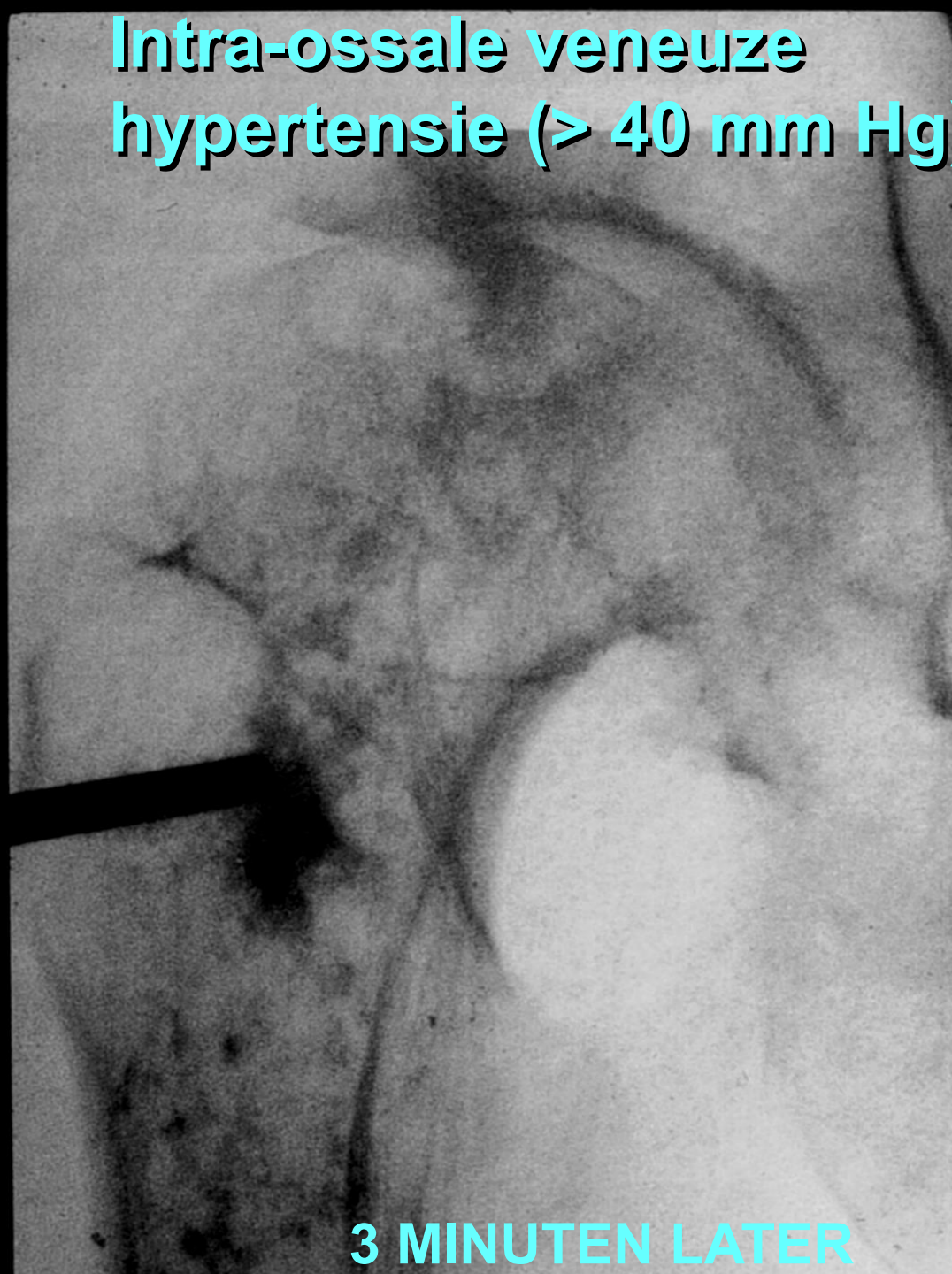


R

CONTRAST INSPUITEN

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S

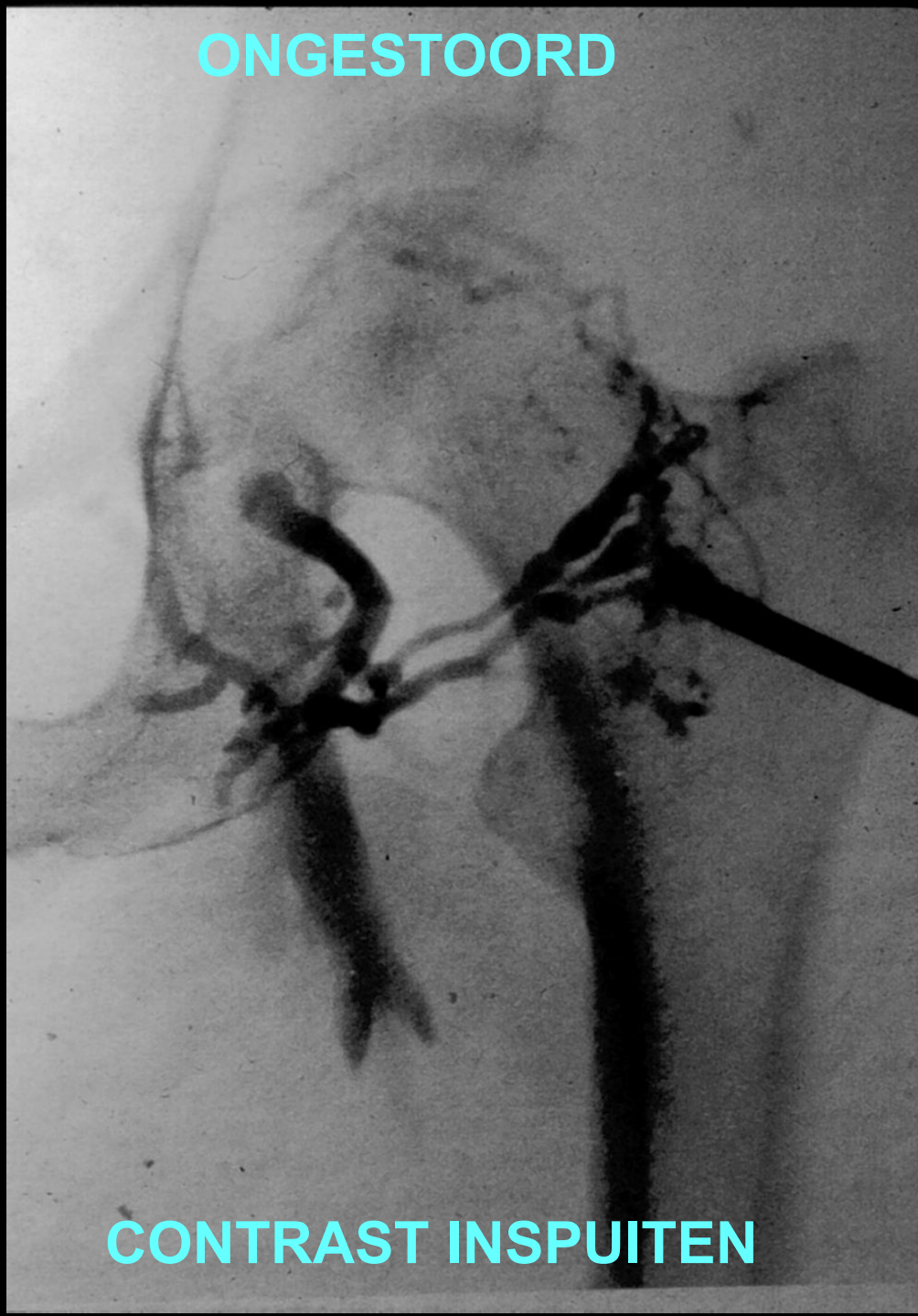
D
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F
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M
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S



Intra-ossale veneuze
hypertensie (> 40 mm Hg)

3 MINUTEN LATER

ONGESTOORD



CONTRAST INSPUITEN

ARTHROSIS DEFORMANS



R

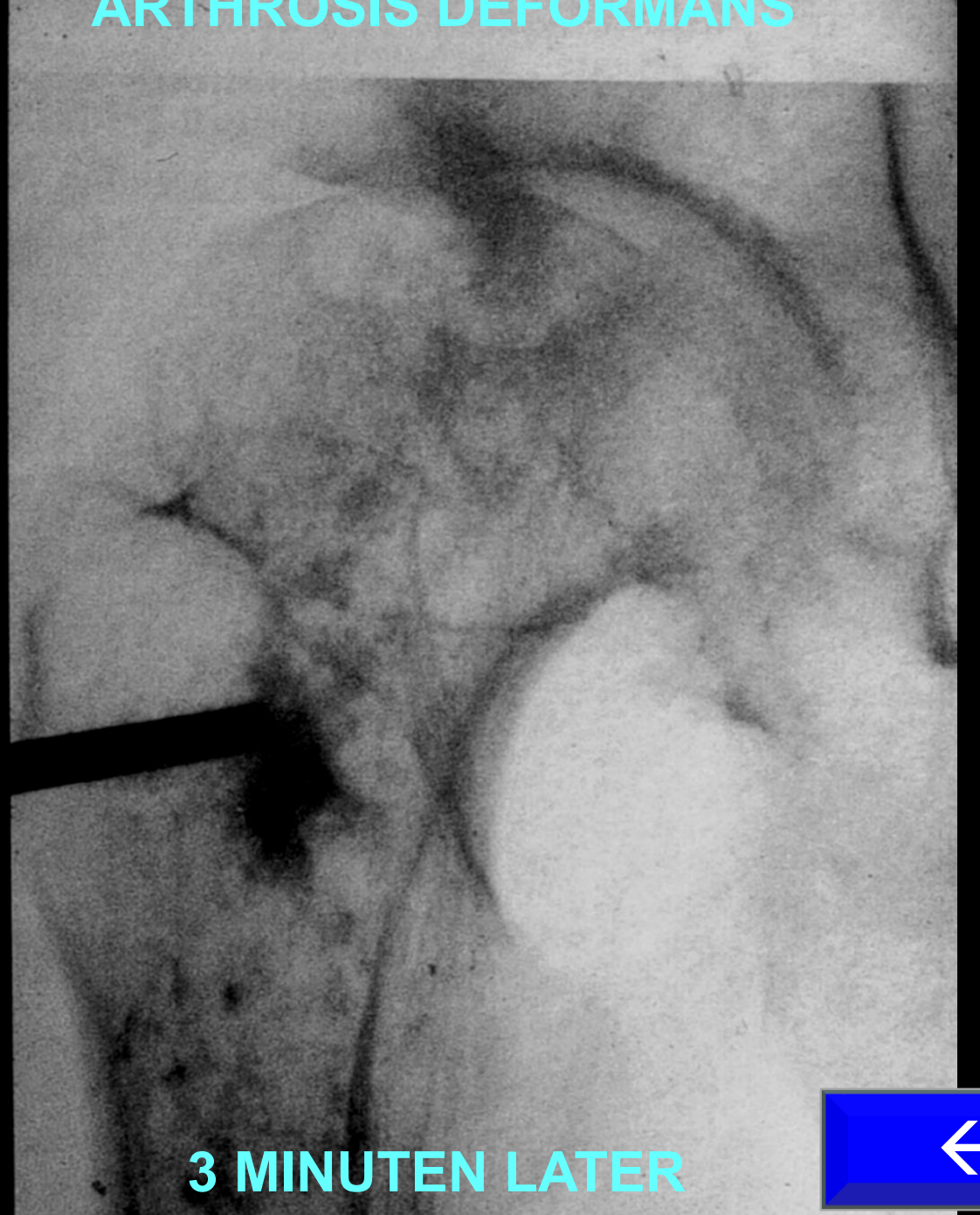
CONTRAST INSPUITEN

ONGESTOORD



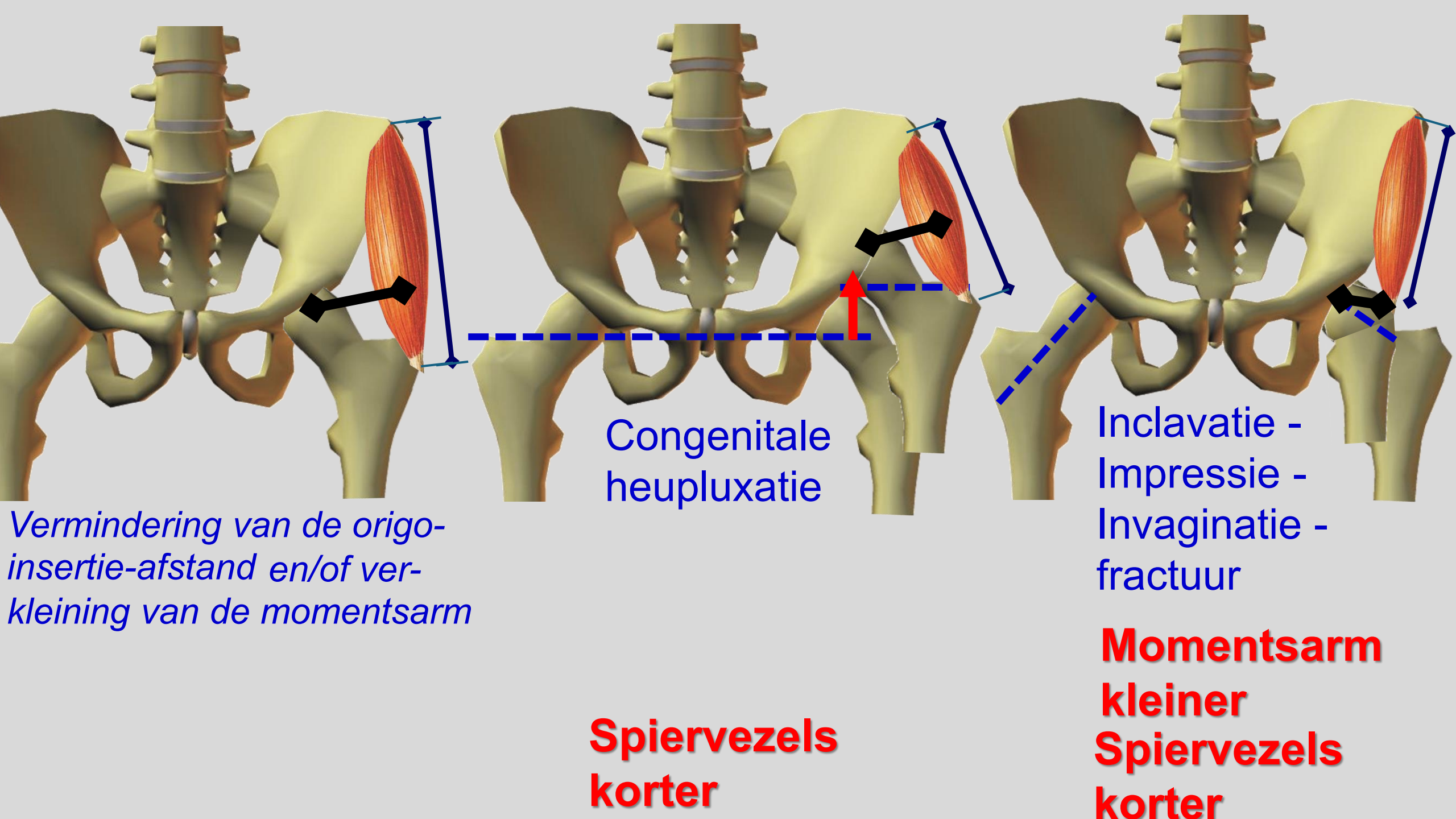
3 MINUTEN LATER

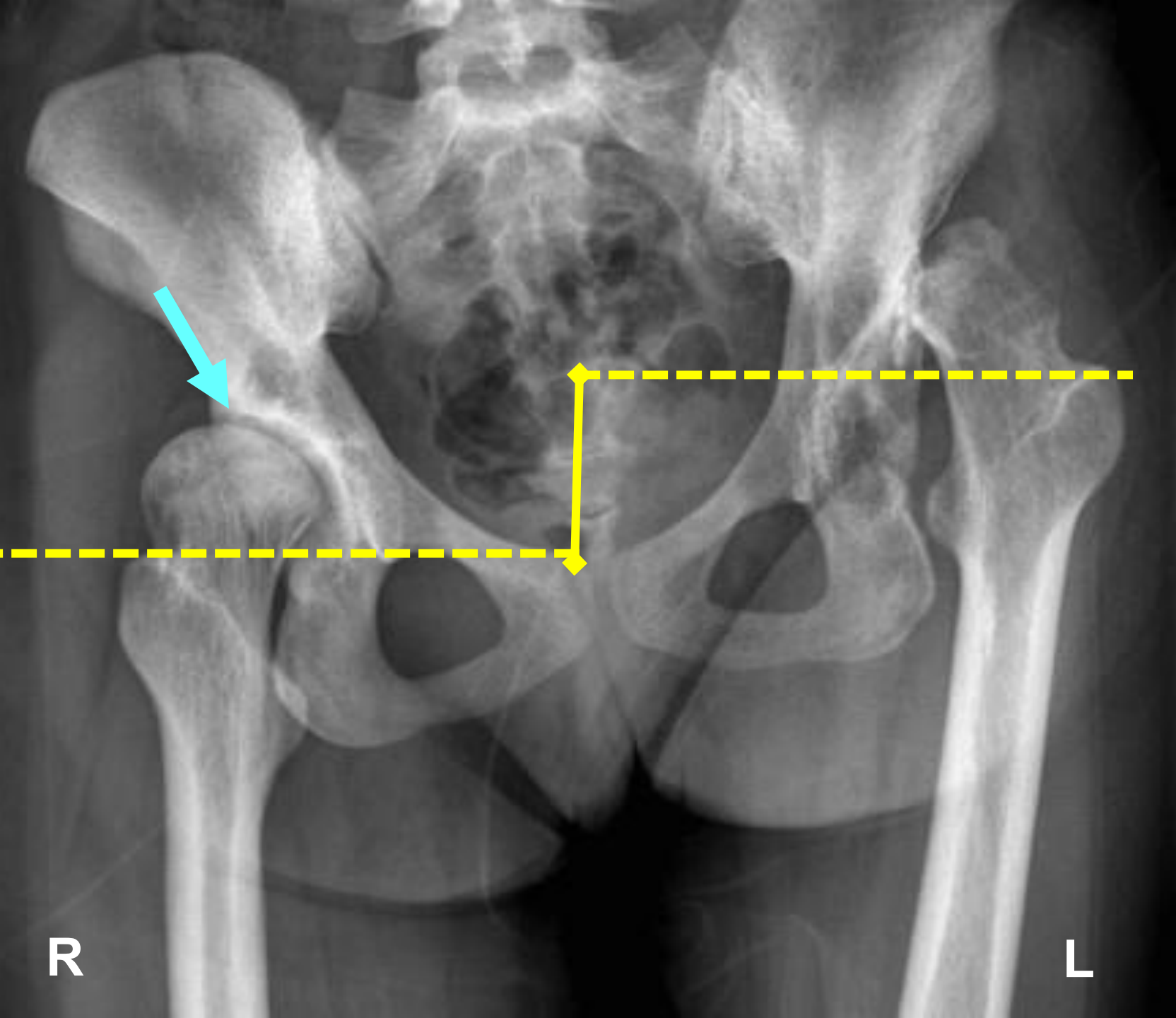
ARTHROSIS DEFORMANS



3 MINUTEN LATER







Congenitale
heupluxatie links.

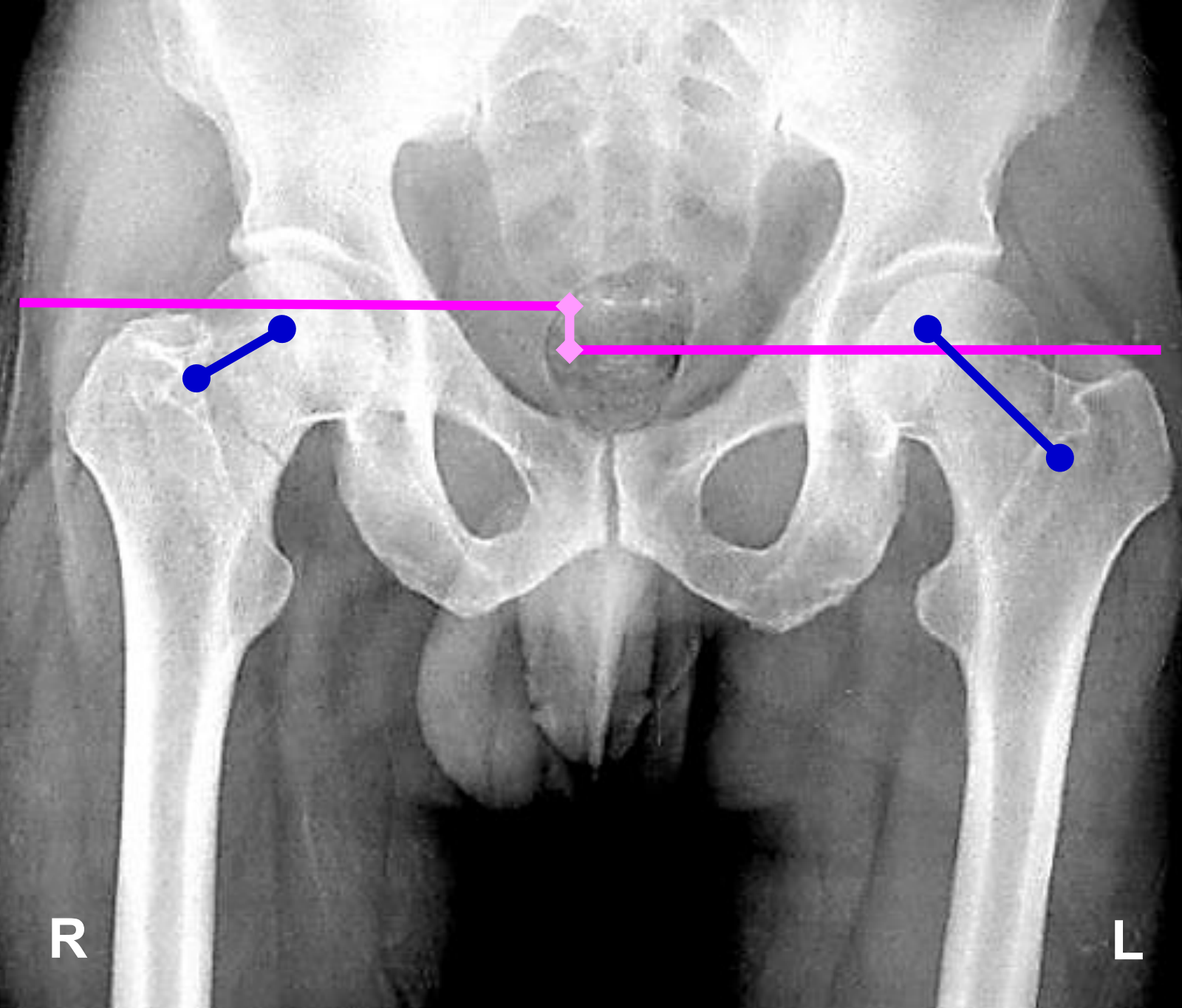
(Rechts steil acetabulum,
verminderde dekking kop
door acetabulum).

Origo-insertieafstand
abductoren links kleiner
dan rechts.



Spiervezel lengte
abductoren links < rechts

<http://www.svuhradiolog.ie/case-study/developmental-dysplasia-of-hips/>



Inclavatiefractuur rechts.

Trochanter major naar craniaal.

Origo - insertie afstand van de abductoren rechts < links

↓
Vezellengten abductoren rechts < links.

Trochanter major naar mediaal.

↓
Momentsarmen abductoren rechts < links.

Effect van de momentsarm op de te leveren spierkracht

$$F_b = 12 \text{ kgf}$$

$$F_s \times 5 = 12 \times 48$$

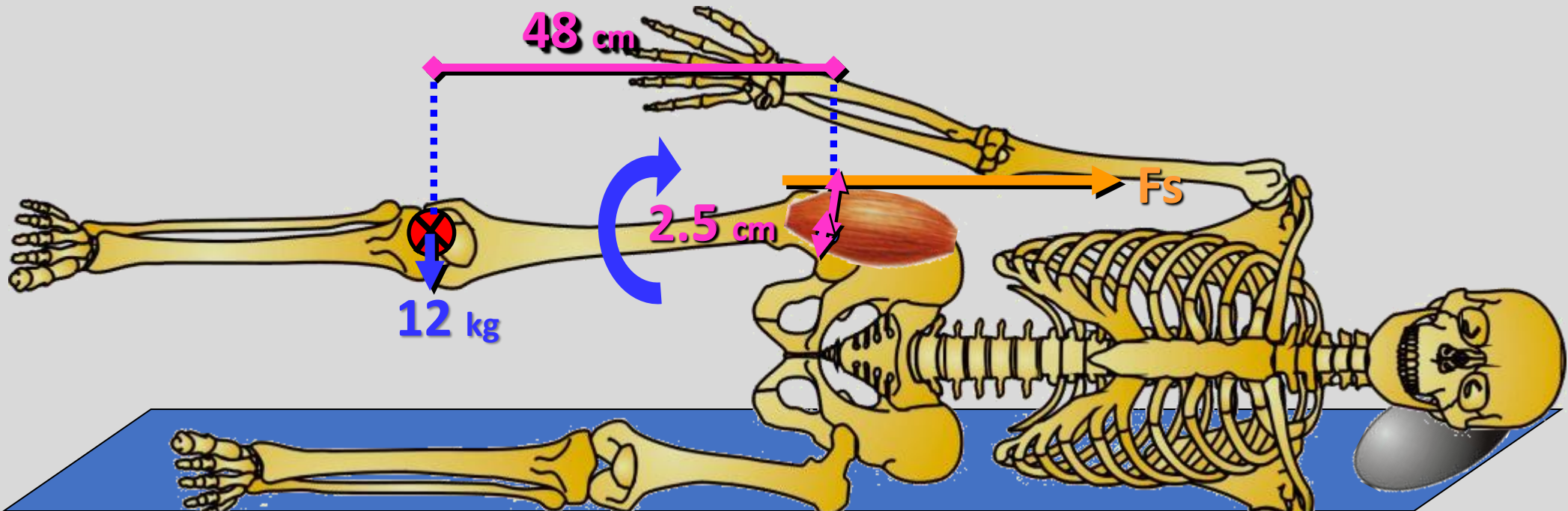
$$F_s = \frac{12 \times 48}{5} = 115 \text{ kgf}$$

$$F_s \approx 10 \times F_b$$

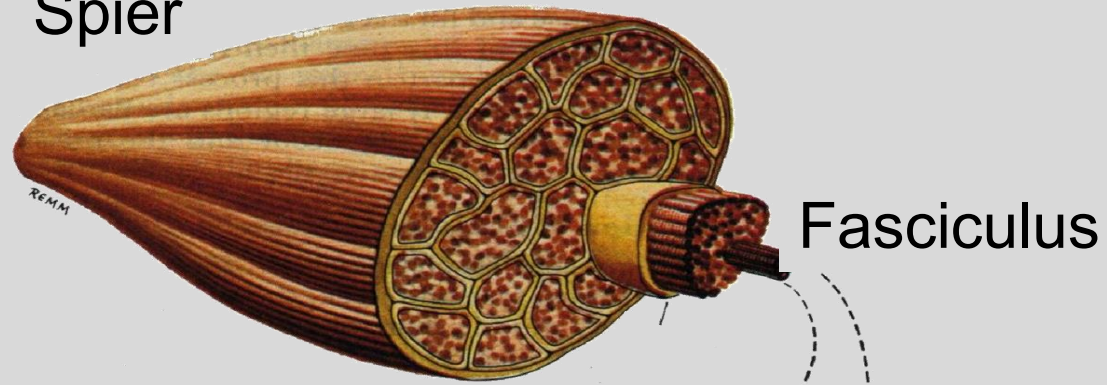
$$F_s \times 2.5 = 12 \times 48$$

$$F_s = \frac{12 \times 48}{2.5} = 230 \text{ kgf}$$

$$F_s \approx 20 \times F_b$$

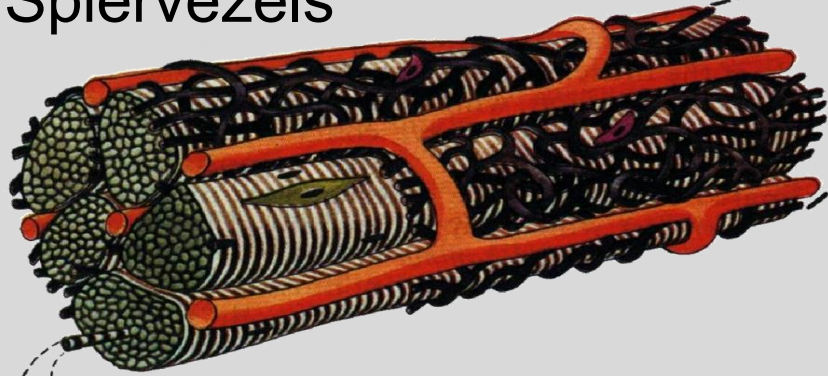


Spier



Fasciculus

Spiervezels

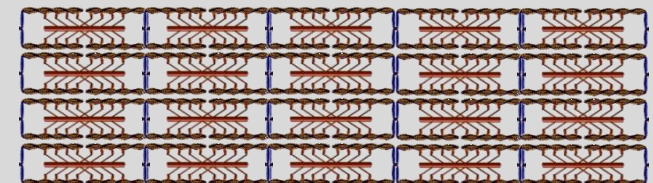
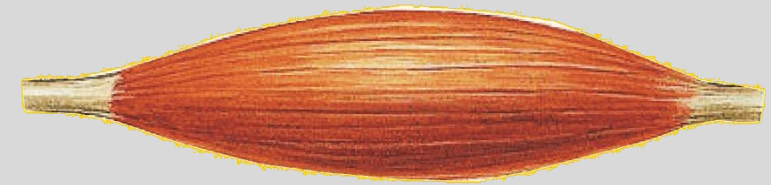
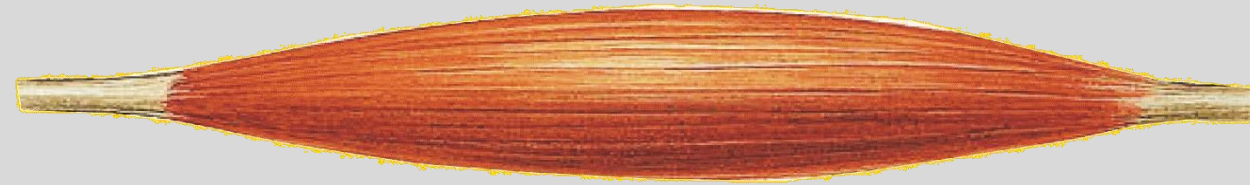


Myofibril

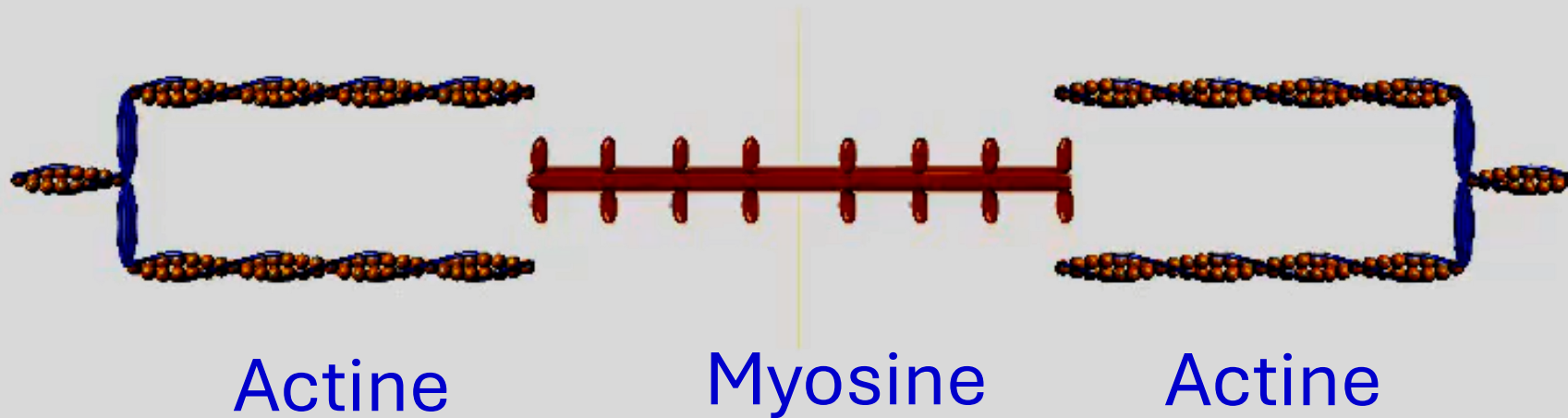
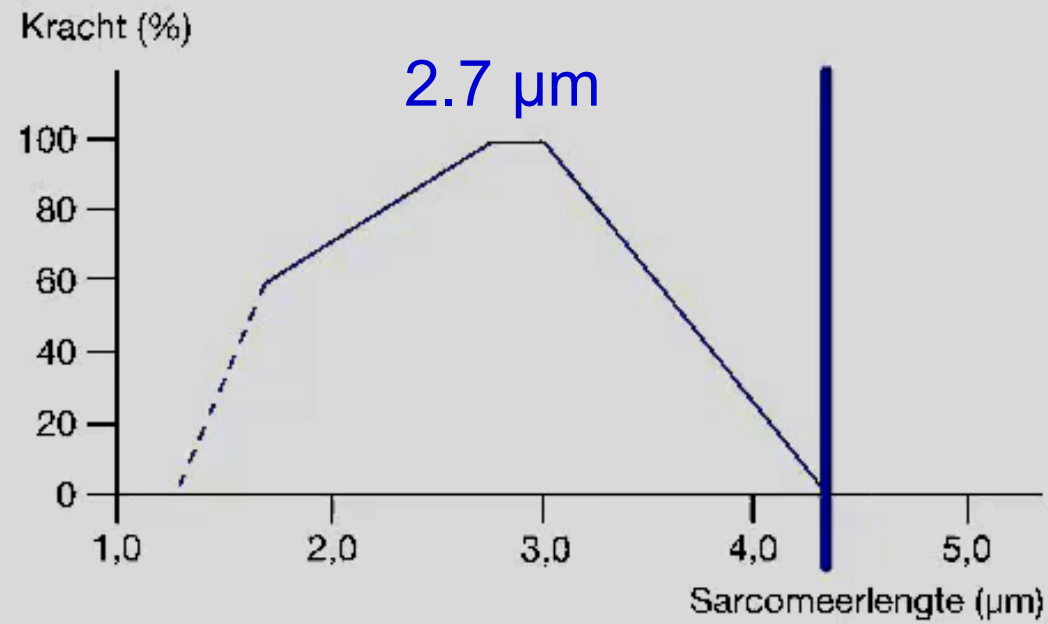
Sarcomeer



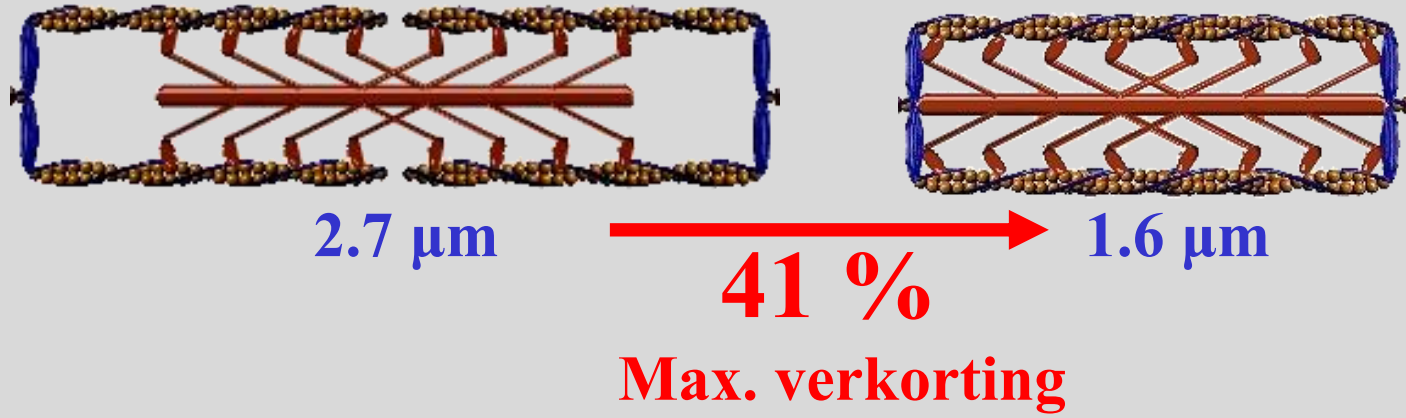
Effect van de vezellengte
op de kracht-lengte relatie



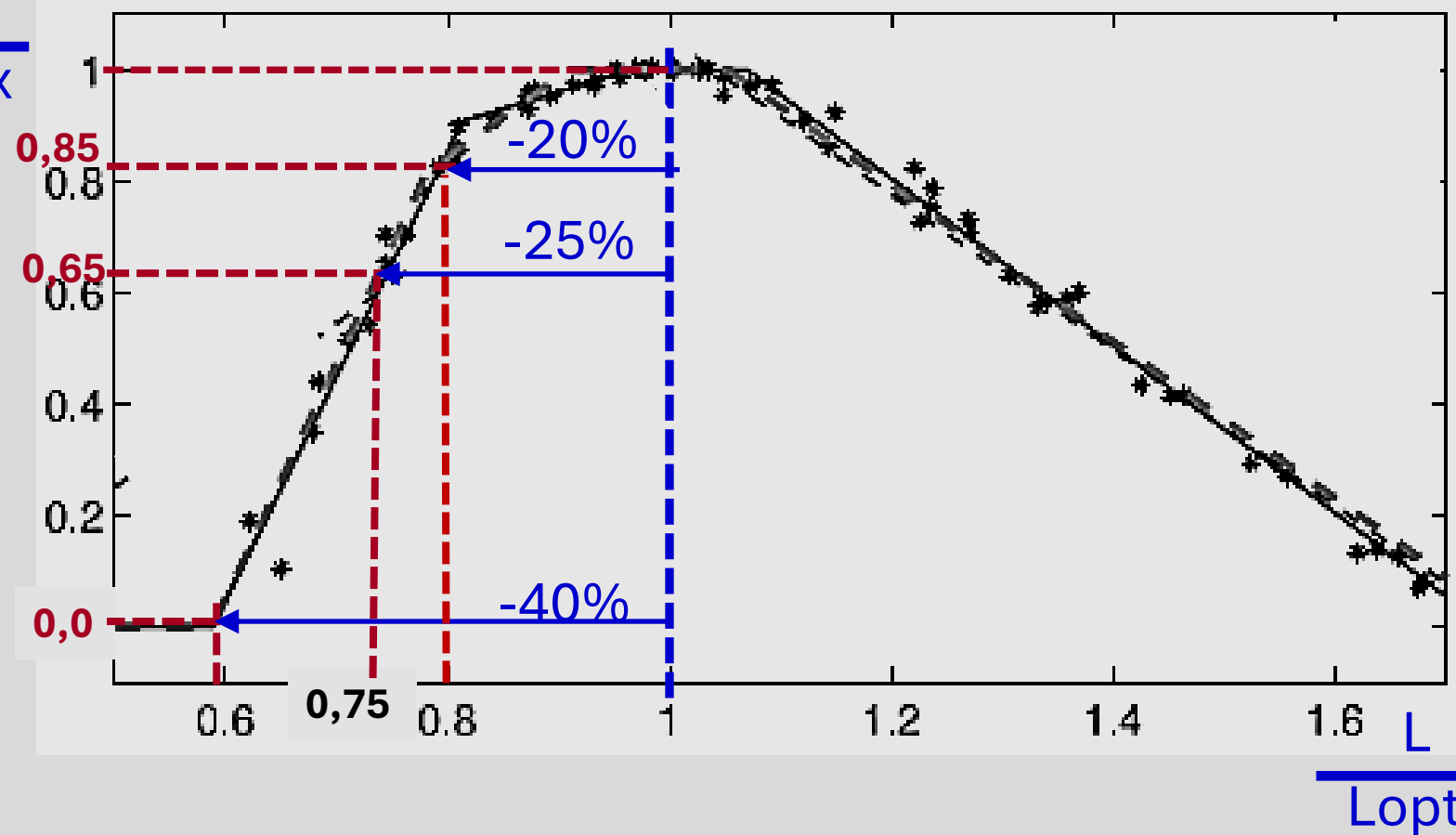
Kracht-Lengte relatie



Verkorting en verlenging vanuit de rustlengte:
 $100 - (\text{Nieuwe Lengte} / \text{Oude Lengte}) \times 100 \%$



$\frac{F}{F_{max}}$



R. Rockenfeller, M. Günther
How to model a muscle's active force-length relation: A comparative study
[Comput. Methods Appl. Mech. Engrg. 313 \(2017\) 321–336](#)

Kracht-Lengte relatie

F_{max} zonder verkorting:

$$3 \times 100 = 300\%$$

F_{max} na verkorting:

$$0 + 65 + 85 = 150\%$$

(gehalveerd)

Stel: spierverskorting = 2 cm

Spier	Vezellengte cm	Verkort %	F _{max} %
M. glut. med.	5	$2/5 \times 100 = 40$	0
M. glut min.	8	$2/8 \times 100 = 25$	65
M. tens. Fasc. Lat.	10	$2/10 \times 100 = 20$	85



Lichaamsgewicht: 74 kg

$F_z = 12 \text{ kg (16\% LG)}$

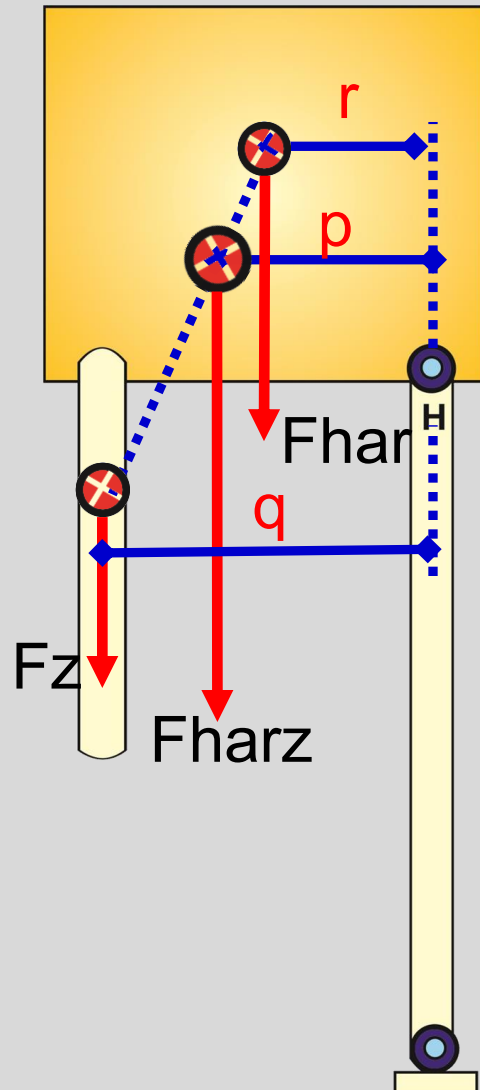
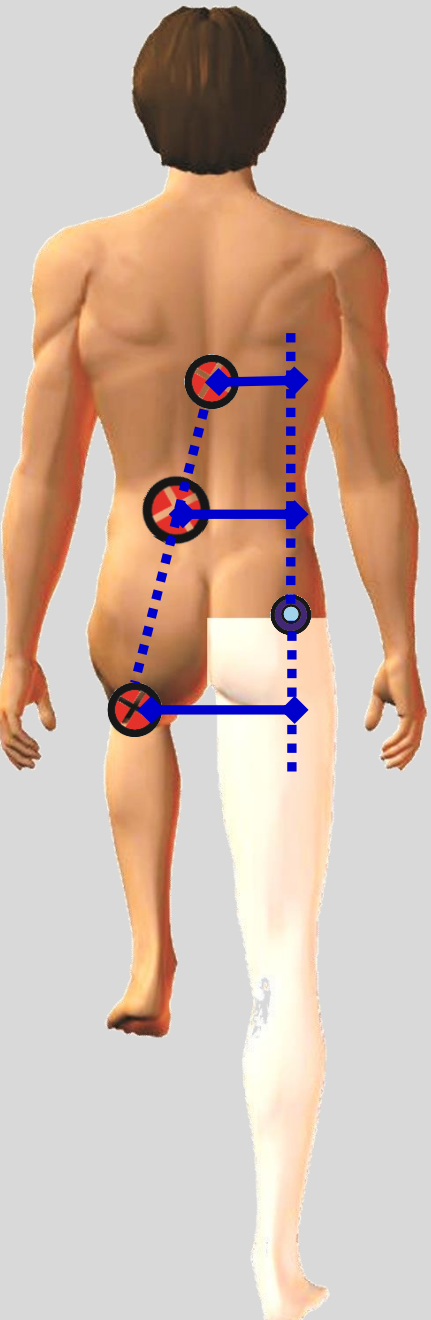
$F_{har} = 74 - (2 \times 12) = 50 \text{ kg}$

$F_{harz} = F_{har} + F_z = 62 \text{ kg}$

$r = 10 \text{ cm}$

$q = 20 \text{ cm}$

$p = ?? \text{ cm}$



$$F_{harz} \times p = F_{har} \times r + F_z \times q$$

$$p = \frac{F_{har} \times r + F_z \times q}{F_{harz}}$$

$$p = \frac{50 \times 10 + 12 \times 20}{62} = 12 \text{ cm}$$



Chirologie

